

Stormwater Report

Dresser Woods New Housing

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Introduction

The Salisbury Housing Committee intends to construct a 20 unit affordable housing project on 5.32 acres at the north end of Railroad Street. Stormwater runoff ultimately reaches Spruce Swamp Creek which lies approximately 400 feet to the east of the site.

Site Description

The property lies in the R-10 Residence Zone with the Multi-Family Housing (MFH) Overlay Zone and is predominately mature forest. There are wetlands and two vernal pools on the north side of the site. The property slopes to the east at varying grades of 3% to 20%. The development occurs in areas of moderate grades generally less than 12%. The underlying non-wetland soils are predominately gravelly sandy loam. The site lies within an aquifer protection area.

Stormwater runoff leaves the site in an easterly direction through three broad swales that lead to Spruce Swamp Creek. For purposes of this report and the accompanying calculations, the discharges are broken down as follows:

The <u>Southerly Watershed</u>: This watershed collects runoff from the southern portion of the site and releases it to a broad swale that leads into the East Meadow neighborhood and then to Spruce Swamp Creek.

The <u>Easterly Watershed</u>: This watershed collects runoff from a small portion of the east side of site and releases it to a wooded area that flows through open space and then to Spruce Swamp Creek.

The <u>Vernal Pool Watershed</u>: This watershed collects runoff from the northern portion of the site and releases it to the on-site wetlands and then to through an open space area and eventually to Spruce Swamp Creek.

Proposed Project

The project involves the construction of nine buildings housing 20 units of housing. Eight of the buildings have two units each and one has four units. The project will include 21 paved parking spaces and 10 overflow parking spaces on a grass paver system. There will be a network of bituminous sidewalks for pedestrian travel.

Stormwater Management Practices

The project uses the following stormwater management practices:

 Reduced impervious coverage to minimize changes in hydrology, some of the parking spaces use a grass paver system to reduce the extent of pavement

- Rain gardens to treat the first inch of runoff from seven out of the nine buildings.
 The remaining two buildings direct their downspouts to splashpads and flow overland. All of the buildings that direct runoff toward the vernal pools have rain gardens.
- The parking area and a substantial portion of the other developed areas of the site are directed to a FocalPoint treatment system. The FocalPoint is a modular treatment system that includes plantings and a high-performance filter media.
- A subsurface detention system reduces peak flows to acceptable levels. Level spreaders are used at each discharge point.
- Minimal disturbance of the 100-foot vernal pool envelope.

There are two underground detention basins. One collects runoff from the majority of the developed portion of the site and releases it to the southerly watershed. A second detention basin collects runoff from the far western developed portion of the site and releases it to the northern end of the vernal pool watershed. The basins have been sized to maintain predevelopment peak flow rates for the 2, 10, 25, 50, and 100-year storm events. Pretreatment for the larger detention basin is provided by the FocalPoint System. Pretreatment for the smaller detention basin is provided by a rain garden.

The outflow from the detention basins are directed to level spreaders before draining into the woods. Detention basin outflow will accumulate in the galleries and discharge through the manufactured openings in the downstream face of the galleries. This facility will spread detention-basin outflow over a wide area at the point of discharge to minimize flow velocity and depth.

Summary of Results

The pre-development and post-development peak discharge rates are presented in the following tables:

Combined Hydrographs

Reccurance Interval	FIOW		Δ Post - Pre
2 Year	2.3	2.2	-0.1
10 Year	3.9	3.7	-0.2
25 Year	4.8	4.6	-0.2
50 Year	5.4	5.2	-0.2
100 Year	6.1	5.9	-0.2

Vernal Pool Watershed

Reccurance Interval Pre-Development		Post Development Flow	Δ Post - Pre	
2 Year	1.9	1.9	0.0	
10 Year	3.1	3.1	0.0	
25 Year	3.8	3.9	0.1	
50 Year	4.3	4.4	0.1	
100 Year	6.1	4.9	-1.2	

Southerly Watershed

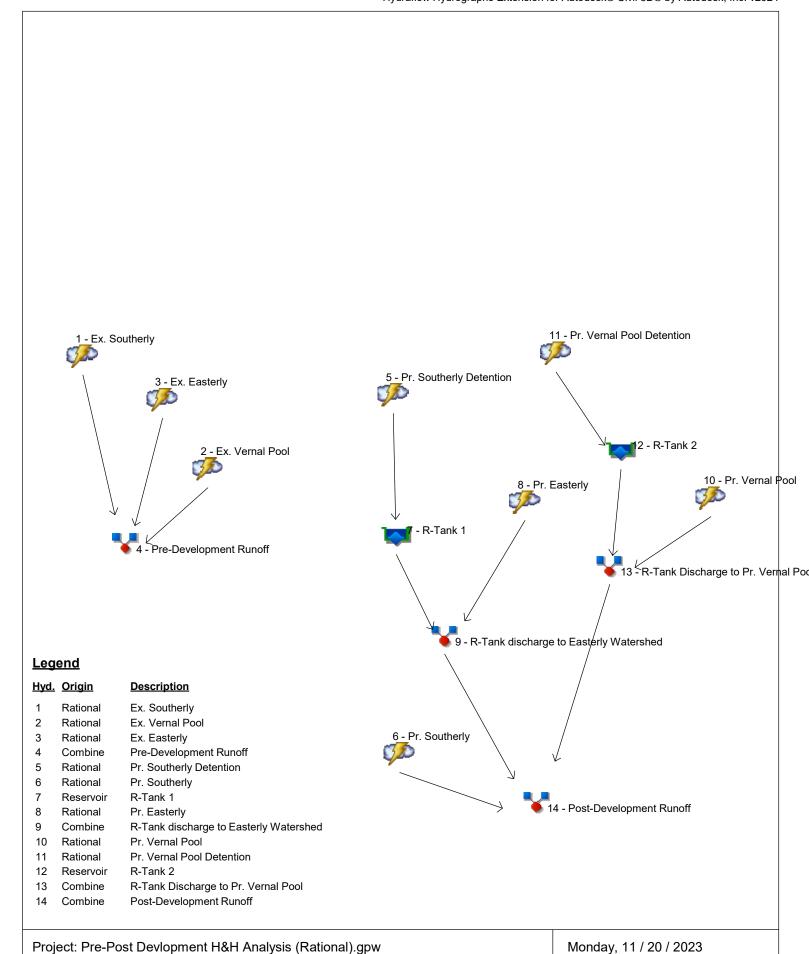
Recurence Interval Pre-Development Flow		Post Development Flow	Δ Post - Pre	
2 Year	0.5	0.2	-0.3	
10 Year	0.9	0.3	-0.6	
25 Year	1.0	0.4	-0.6	
50 Year	1.2	0.5	-0.7	
100 Year	1.3	0.5	-0.8	

Easterly Watershed

Easterly Watershed								
Recurence Interval	Pre-Development Flow	Post Development Flow	Δ Post - Pre					
2 Year	0.03	0.5	0.5					
10 Year	0.05	0.8	0.8					
25 Year	0.06	1.0	0.9					
50 Year	0.06	1.1	1.1					
100 Year	0.07	1.3	1.2					

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Watershed Model Schematic



B. Hydrologic Input

Tc Calculations
CN Calculations

Watershed Maps



SUBJECT: Time of Concentration Calculation

COMP. BY: CG CHK. BY: TAP DATE: 11/20/23

Watershed I.D.: Existing Southerly Watershed

Estimate Time of Concentration using the "Velocity Method".

Reference: USDA-NRCS National Engineering Handbook - Part 630 -Hydrology; Chapter 15 - Time of Concentration and USDA-NRCS TR-55 - June 1986

SHEET FLOW

Step No.	Data	Seg. I.D.:	1	Seg. I.D.:	2
1A	Select Surface Description Identifier (Table 3-1)		I		
1B	Surface Description (Table 3-1)	Woods: Ligh	t Underbrush		
2	Manning's Roughness Coefficient "n" (Table 3-1)	0.4	0.400		
3	Flow Length "L" (FT) - Note: Total L must be <= 100 FT	27	27.5		
4	Two-Year 24-Hour Rainfall "P ₂ " (Inches)	3	.1		
5	Land Slope "S" (FT / FT)	0.0	030		
6	Travel Time "T _T " (Hours)	0.1	110		

$$T_{T} = \frac{0.007 \times (n \times L)^{0.8}}{P_{2}^{0.5} \times S^{0.4}}$$

NRCS TR-55 Table 3-1

		Manning's
Identifier	Surface Description	"n"
Α	Smooth Surfaces (Conc., Asph., Grav., Bare Soil)	0.011
В	Fallow (No Residue)	0.050
С	Cultivated Soils (Residue Cover <= 20%)	0.060
D	Cultivated Soils (Residue Cover > 20%)	0.170
E	Grass: Short Grass Prairie	0.150
F	Grass: Dense Grasses	0.240
G	Grass: Bermuda Grass	0.410
Н	Range (Natural)	0.130
I	Woods: Light Underbrush	0.400
J	Woods: Dense Underbrush	0.800

SHALLOW CONCENTRATED FLOW

		Segment I.D.					
Step No.	Data	3	4	5	6	7	8
7	Surface Description (Paved or Unpaved)	U	U				
8	Flow Length "L" (FT)	103	54				
9	Watercourse Slope "S" (FT/FT)	0.0270	0.0900				
10	Average Velocity "V" (FT/SEC) Figure 3-1	2.65	4.84				
11	Travel Time "T _T " (Hours)	0.011	0.003				
-	L Unpaved Condition:		Paved Condi	ition:	•	T _T =	0.014

$$T_T = \frac{L}{3600 \text{ x V}}$$
 Unpaved Condition: Paved Condition: $V = 16.1345 \text{ x S}^{0.5}$ $V = 20.3282 \text{ x S}^{0.5}$



SUBJECT: Time of Concentration Calculation

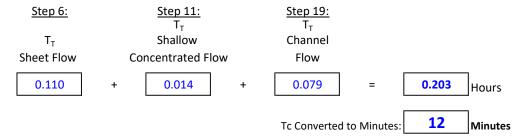
COMP. BY: CG CHK. BY: TAP DATE: 11/20/23

OPEN CHANNEL FLOW

Note: Hydraulic properties estimated from the worksheets that follow below.

					Segment I.D.			
Step No.	Data	9	10	11	12	13	14	15
12A	Channel or Pipe Flow? (C or P)	С	С	С				
12B	Cross Sectional Flow Area (SF)	0.19	0.22	0.30				
13	Wetted Perimeter (FT)	3.41	3.61	4.01				
14	Hydraulic Radius (FT)	0.06	0.06	0.07				
14	Channel or Pipe Slope (FT/FT)	0.0140	0.0190	0.0220				
16	Manning's Roughness Coefficient	0.024	0.024	0.024				
17	Velocity (FT/SEC)	1.07	1.34	1.63				
18	Flow Length (L) (FT)	148	108	104				
19	Travel Time "T _T " (Hours)	0.039	0.022	0.018				
	T ₊ =L						T _T =	0.079
	3600 x V						-	

Step 20: Watershed Time of Concentration (Add T_T from Steps 6, 11, and 19):



Notes:

- 1. The sum of all sheet-flow travel lengths is <= 100 FT as recommended in NRCS NEH Part 630 Chapter 15.
- 3. The sum of sheet-flow travel length is <= 10% of total hydraulic length (OK)
- 3. The sheet flow travel time is less than 80% of Tc (OK)
- 4. The sum of shallow-concentrated flow segment lengths is < 1,000 FT (OK)



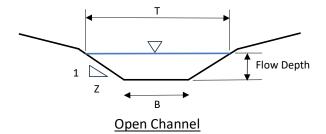
SUBJECT: Time of Concentration Calculation

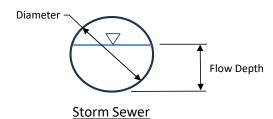
COMP. BY: CG CHK. BY: TAP DATE: 11/20/23

The following worksheets estimate velocity and flow rate for a channel with simple geometry or a round storm sewer. The calculations are used to estimate travel time for open-channel flow conditions. Individual segments may be either channel flow or pipe flow, but not both.

Notes:

- 1. Flow rate in the various segments should gradually build (in general proportion to drainage area) toward the computed two-year recurrence-interval flood at the point of analysis.
- 2. In the case of flow in natural or man-made channels, flow depth should not exceed bank-full height.





Open Channel Segments

					Segment I.D.			
	Item	9	10	11	12	13	14	15
	Flow Depth (FT)	0.07	0.08	0.10				
itry	Channel Slope (FT/FT)	0.0140	0.0190	0.0220				
Channel Geometry	Manning's Roughness Coefficient	0.024	0.024	0.024				
G G	Bank Slope (Z:1)	10.00	10.00	10.00				
	B - Channel Base Width (FT)	2.00	2.00	2.00				
	T - Flow Top Width (FT)	3.4	3.6	4				
_ s	Flow Area (SF)	0.19	0.22	0.30				
auli auli	Wetted Perimeter (FT)	3.41	3.61	4.01				
Channel Hydraulics	Hydraulic Radius (FT)	0.06	0.06	0.07				
O É	Flow (CFS)	0.20	0.30	0.49				
	Average Velocity (FT/SEC)	1.07	1.34	1.63				

Pipe Segments

-		Segment I.D.						
	Item	9	10	11	12	13	14	15
S	Pipe Diameter (FT)							
istic	Pipe Manning's Coefficient							
Characteristics	Pipe Slope (FT/FT)							
rac	Full Pipe Area (SF)							0.0000
Chã	Hydraulic Radius - Full Pipe (FT)							0.000
Pipe	Q _{FULL} - Full Pipe Flow (CFS)							#DIV/0!
Ξ	V _{FULL} - Full Pipe Velocity (FT/SEC)							#DIV/0!
	R _D - Flow Depth Ratio							
	Flow Depth (FT)							0.00
ics	Cross Sectional Area of Flow (SF)							0.000
Pipe Hydraulics	Wetted Perimeter (FT)							0.000
lydı	Hydraulic Radius (FT)							0.000
ē T	Q - Estimated Flow in Pipe (CFS)							0.00
Pip	V - Estimated Velocity in Pipe (FT/SEC)							0.00
	Q / Q _{FULL}							0.00
	V / V _{FULL}							0.00



SUBJECT: Time of Concentration Calculation

COMP. BY: CG CHK. BY: TAP DATE: 11/20/23

Watershed I.D.: Vernal Pool Watershed

Estimate Time of Concentration using the "Velocity Method".

Reference: USDA-NRCS National Engineering Handbook - Part 630 -Hydrology; Chapter 15 - Time of Concentration and USDA-NRCS TR-55 - June 1986

SHEET FLOW

Step No.	Data	Seg. I.D.:	1	Seg. I.D.:	2
1A	Select Surface Description Identifier (Table 3-1)		Ī		
1B	Surface Description (Table 3-1)	Woods: Ligh	t Underbrush		
2	Manning's Roughness Coefficient "n" (Table 3-1)	0.4	0.400		
3	Flow Length "L" (FT) - Note: Total L must be <= 100 FT	2	22		
4	Two-Year 24-Hour Rainfall "P ₂ " (Inches)	3	.1		
5	Land Slope "S" (FT / FT)	0.0	013		
6	Travel Time "T _T " (Hours)	0.3	129		

$$T_{T} = \frac{0.007 \times (n \times L)^{0.8}}{P_{2}^{0.5} \times S^{0.4}}$$

NRCS TR-55 Table 3-1

		Manning's
Identifier	Surface Description	"n"
Α	Smooth Surfaces (Conc., Asph., Grav., Bare Soil)	0.011
В	Fallow (No Residue)	0.050
С	Cultivated Soils (Residue Cover <= 20%)	0.060
D	Cultivated Soils (Residue Cover > 20%)	0.170
E	Grass: Short Grass Prairie	0.150
F	Grass: Dense Grasses	0.240
G	Grass: Bermuda Grass	0.410
Н	Range (Natural)	0.130
I	Woods: Light Underbrush	0.400
J	Woods: Dense Underbrush	0.800

SHALLOW CONCENTRATED FLOW

		Segment I.D.									
Step No.	Data	3	4	5	6	7	8				
7	Surface Description (Paved or Unpaved)	U	U	U	C						
8	Flow Length "L" (FT)	259	19.4	76.74	64.15						
9	Watercourse Slope "S" (FT/FT)	0.0130	0.2660	0.0420	0.2470						
10	Average Velocity "V" (FT/SEC) Figure 3-1	1.84	8.32	3.31	8.02						
11	Travel Time "T _T " (Hours)	0.039	0.001	0.006	0.002						
-	L Unpaved Condition:		Paved Cond	ition:		T _T =	0.048				

$$T_T = \frac{L}{3600 \times V}$$
 Unpaved Condition: Paved Condition: $V = 16.1345 \times S^{0.5}$ $V = 20.3282 \times S^{0.5}$



SUBJECT: Time of Concentration Calculation

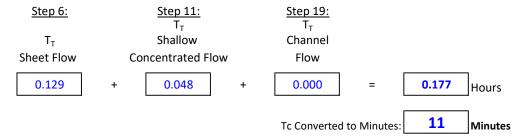
COMP. BY: CG CHK. BY: TAP DATE: 11/20/23

OPEN CHANNEL FLOW

Note: Hydraulic properties estimated from the worksheets that follow below.

					Segment I.D.			
Step No.	Data	9	10	11	12	13	14	15
12A	Channel or Pipe Flow? (C or P)							
12B	Cross Sectional Flow Area (SF)							
13	Wetted Perimeter (FT)							
14	Hydraulic Radius (FT)							
14	Channel or Pipe Slope (FT/FT)							
16	Manning's Roughness Coefficient							
17	Velocity (FT/SEC)							
18	Flow Length (L) (FT)							
19	Travel Time "T _T " (Hours)							
	T _ L		•	•	•		T _T =	0.000
	$T_{T} = \frac{L}{3600 \times V}$						T _T =	

Step 20: Watershed Time of Concentration (Add T_T from Steps 6, 11, and 19):



Notes:

- 1. The sum of all sheet-flow travel lengths is <= 100 FT as recommended in NRCS NEH Part 630 Chapter 15.
- 2. The sum of sheet-flow travel length is <= 10% of total hydraulic length (OK)
- 3. The sheet flow travel time is less than 80% of Tc (OK)
- 4. The sum of shallow-concentrated flow segment lengths is < 1,000 FT (OK)



SUBJECT: Time of Concentration Calculation

COMP. BY: CG CHK. BY: TAP DATE: 11/20/23

Watershed I.D.: Proposed Southerly Detention Watershed

Estimate Time of Concentration using the "Velocity Method".

Reference: USDA-NRCS National Engineering Handbook - Part 630 -Hydrology; Chapter 15 - Time of Concentration and USDA-NRCS TR-55 - June 1986

SHEET FLOW

Step No.	Data	Seg. I.D.:	1	Seg. I.D.:	2	
1A	Select Surface Description Identifier (Table 3-1)	i				
1B	Surface Description (Table 3-1)	Woods: Light	Woods: Light Underbrush			
2	Manning's Roughness Coefficient "n" (Table 3-1)	0.4	.00			
3	Flow Length "L" (FT) - Note: Total L must be <= 100 FT	3	36			
4	Two-Year 24-Hour Rainfall "P ₂ " (Inches)	3.	1			
5	Land Slope "S" (FT / FT)	0.0	30			
6	Travel Time "T _T " (Hours)	0.1	37			

$$T_{T} = \frac{0.007 \times (n \times L)^{0.8}}{P_{2}^{0.5} \times S^{0.4}}$$

NRCS TR-55 Table 3-1

IVINCO TIN-DO	Table 3 1	
		Manning's
Identifier	Surface Description	"n"
Α	Smooth Surfaces (Conc., Asph., Grav., Bare Soil)	0.011
В	Fallow (No Residue)	0.050
С	Cultivated Soils (Residue Cover <= 20%)	0.060
D	Cultivated Soils (Residue Cover > 20%)	0.170
E	Grass: Short Grass Prairie	0.150
F	Grass: Dense Grasses	0.240
G	Grass: Bermuda Grass	0.410
Н	Range (Natural)	0.130
I	Woods: Light Underbrush	0.400
J	Woods: Dense Underbrush	0.800

SHALLOW CONCENTRATED FLOW

		Segment I.D.								
Step No.	Data	3	4	5	6	7	8			
7	Surface Description (Paved or Unpaved)	U	Р	U						
8	Flow Length "L" (FT)	149	175	46						
9	Watercourse Slope "S" (FT/FT)	0.0400	0.0200	0.0400						
10	Average Velocity "V" (FT/SEC) Figure 3-1	3.23	2.87	3.23						
11	Travel Time "T _T " (Hours)	0.013	0.017	0.004						
-	L Unpaved Condition:		Paved Cond	ition:		T _T =	0.034			

$$T_T = \frac{L}{3600 \text{ x V}}$$
 Unpaved Condition: Paved Condition: $V = 16.1345 \text{ x S}^{0.5}$ $V = 20.3282 \text{ x S}^{0.5}$



SUBJECT: Time of Concentration Calculation

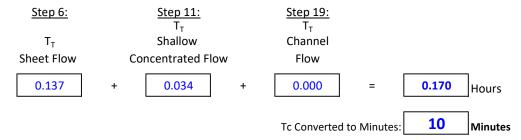
COMP. BY: CG CHK. BY: TAP DATE: 11/20/23

OPEN CHANNEL FLOW

Note: Hydraulic properties estimated from the worksheets that follow below.

					Segment I.D.	1		
Step No.	Data	9	10	11	12	13	14	15
12A	Channel or Pipe Flow? (C or P)							
12B	Cross Sectional Flow Area (SF)							
13	Wetted Perimeter (FT)							
14	Hydraulic Radius (FT)							
14	Channel or Pipe Slope (FT/FT)							
16	Manning's Roughness Coefficient							
17	Velocity (FT/SEC)							
18	Flow Length (L) (FT)							
19	Travel Time "T _T " (Hours)							
	T_ = L	•	•	•	•	•	T _T =	0.000
	3600 x V							

Step 20: Watershed Time of Concentration (Add T_T from Steps 6, 11, and 19):



Notes:

- 1. The sum of all sheet-flow travel lengths is <= 100 FT as recommended in NRCS NEH Part 630 Chapter 15.
- 3. The sum of sheet-flow travel length is <= 10% of total hydraulic length (OK)
- 3. The sheet flow travel time exceeds 80% of Tc. Consider reducing sheet flow length(s).
- 4. The sum of shallow-concentrated flow segment lengths is < 1,000 FT (OK)



PROJECT: Dresser Woods - Railroad Street - Salisbury, CT

SUBJECT: Runoff Coefficient Worksheet

COMP. BY: CG CHK. BY: TAP DATE: 11/20/23

Runoff Coefficients per ConnDOT Drainage Manual - Chapter 6:

Table 6-3 - Recommended Coefficients for Pervious Areas:

		NRCS Hydro	ologic Soil Grou	р
Slope	Α	В	C	D
Flat: (0%-1%)	0.04 - 0.09	0.07 - 0.12	0.11 - 0.16	0.15 - 0.20
Ave.: (2%-6%)	0.09 - 0.14	0.12 - 0.17	0.16 - 0.21	0.20 - 0.25
Steep: (> 6%)	0.13 - 0.18	0.18 - 0.24	0.23 - 0.31	0.28 - 0.38

<u>Table 6-5 - Runoff Coefficients for Impervious Areas</u>

Asphalt	Concrete	Drives &	
Streets	Streets Streets		Roofs
0.70 - 0.95	0.80 - 0.95	0.75 - 0.85	0.75 - 0.95

<u>Table 6-4 - Recommended Coefficients for Various Selected Land Uses:</u>

	Neighbor-	Single	Multi	Multi		Resi-	Apartment	Light	Heavy	Parks &		Rail	Un-
Downtown	hood	Family	Units	Units		dential	Dwelling	Industrial	Industrial	Cemetery	Play-	Yard	Improved
Areas	Areas	Areas	Detached	Attached	Suburban	(>1.2 Ac.)	Areas	Areas	Areas		grounds	Areas	Areas
0.70 - 0.95	0.50 - 0.70	0.30 - 0.50	0.40 - 0.60	0.60 - 0.75	0.25 - 0.40	0.30 - 0.45	0.50 - 0.70	0.50 - 0.80	0.60 - 0.90	0.10 - 0.25	0.20 - 0.40	0.20 - 0.40	0.10 - 0.30

Calculate Composite Runoff Coefficient and Adjust for Infrequent Storms:

			Woods	Grass						C _A - Runoff Coefficient Adjusted for Infrequent Storms					
		Impervious	HSG-A	HSG-A	Water	Other	Check		Composite			Recurre	nce Interval		
	Total	(Acres)	(Acres)	(Acre)	(Acres)	(Acres)	S Area		Runoff	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year
Area	Area	C =	C =	C =	C =	C =	(Acres)	SAxC	Coefficient	C _F =	C _F =	C _F =	Max.C _F =	Max.C _F =	Max.C _F =
I.D.	(Acres)	0.90	0.10	0.25	0.90				C'	1.00	1.00	1.00	1.10	1.20	1.25
		Pre	-Development		-							-			
Ex. Southerly	1.95		1.95				1.95	0.195	0.10	0.10	0.10	0.10	0.11	0.12	0.13
Ex. Vernal Pool	4.22		3.91		0.31		4.22	0.670	0.16	0.16	0.16	0.16	0.17	0.19	0.20
Ex. Easterly	0.08		0.08				0.08	0.008	0.10	0.10	0.10	0.10	0.11	0.12	0.13
Toal	6.25	0	5.94	0	0.31										
		Pos	t-Developmen	t											
Pr. Southerly	0.49	0.00	0.44	0.05			0.49	0.057	0.12	0.12	0.12	0.12	0.13	0.14	0.14
Pr. Southerly Detention	1.33	0.62	0.2	0.51			1.33	0.706	0.53	0.53	0.53	0.53	0.58	0.64	0.66
Pr. Vernal Pool	3.75	0.02	3.25	0.17	0.31		3.75	0.665	0.18	0.18	0.18	0.18	0.19	0.21	0.22
Pr. Vernal Pool Detention	0.55	0.1	0.22	0.23			0.55	0.170	0.31	0.31	0.31	0.31	0.34	0.37	0.39
Pr. Easterly	0.30	0.1	0.1	0.1			0.30	0.125	0.42	0.42	0.42	0.42	0.46	0.50	0.52
Toal	6.42	0.84	4.21	1.06	0.31										

- (1) Area of individual cover types measured from plans
- (2) Runoff coefficient for individual cover types selected from reference tables above.
- (3) Composite Runoff Coefficient C' = S(A x C) / SA
- (4) Frequency Factors ($C_{\rm F}$) from ConnDOT Drainage Manual 2000 Table 6-2
- (5) Per ConnDOT Drainage Manual 2000 Section 6.9.5: $C_A = 1.00$ where C'* $C_F >= 1.00$ $C_A = C'* C_F$ where C'* $C_F < 1.00$

FILE LOCATION: P.1CT4010271-QUISENBERRY ARCARI MALIK ARCHITECTS, LLC\(23137 - RAILROAD STREET SALISBURY- TAP\02-CAD_FILES\(CIVIL\H\&H-UNDERGROUND DETENTION.DWG, 2023.11.20, 9:55 AM

FILE LOCATION: P.1CT4010271-QUISENBERRY ARCARI MALIK ARCHITECTS, LLC\(23137 - RAILROAD STREET SALISBURY- TAP\02-CAD_FILES\(CIVIL\H\&H-UNDERGROUND DETENTION.DWG, 2023.11.20, 9:58 AM

C. Hydrographs

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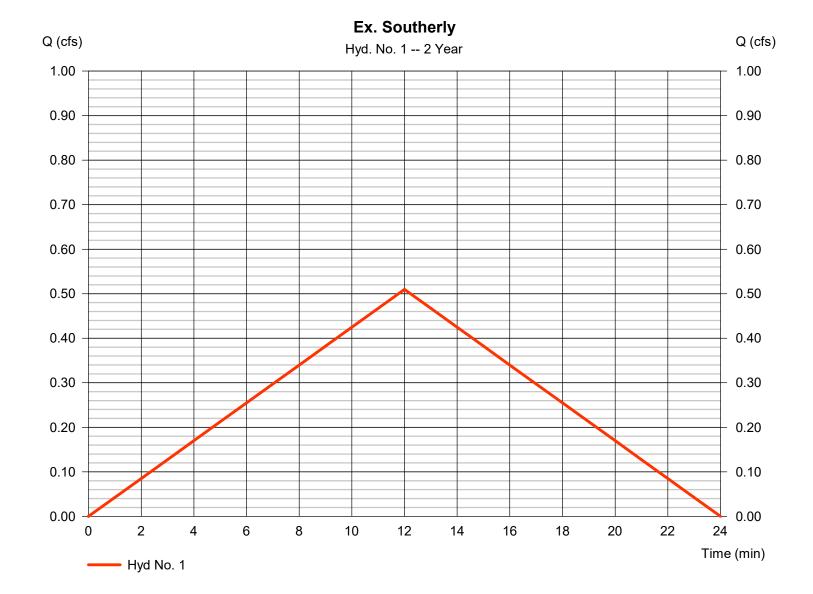
Hyd. No. 1

Ex. Southerly

= Rational Hydrograph type Peak discharge = 0.510 cfsStorm frequency Time to peak = 2 yrs= 12 min Time interval = 1 min Hyd. volume = 367 cuft Drainage area Runoff coeff. = 1.950 ac= 0.1

Intensity = 2.614 in/hr Tc by User = 12.00 min

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Renovemb10 Fract = 1/1



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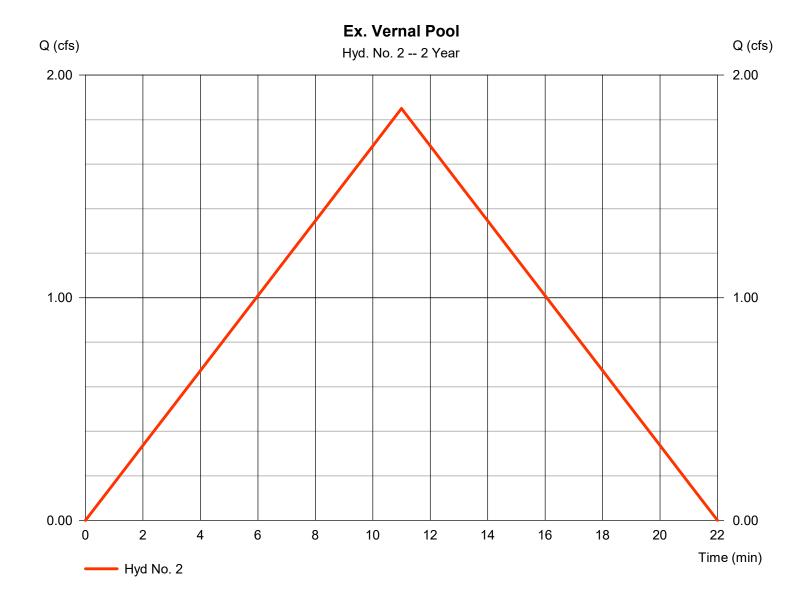
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Hyd. No. 2

Ex. Vernal Pool

Hydrograph type = Rational Peak discharge = 1.850 cfsStorm frequency = 2 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 1,221 cuft Drainage area = 4.220 acRunoff coeff. = 0.16Tc by User = 11.00 min Intensity = 2.740 in/hr

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Exerc/teinhDFfact = 1/1



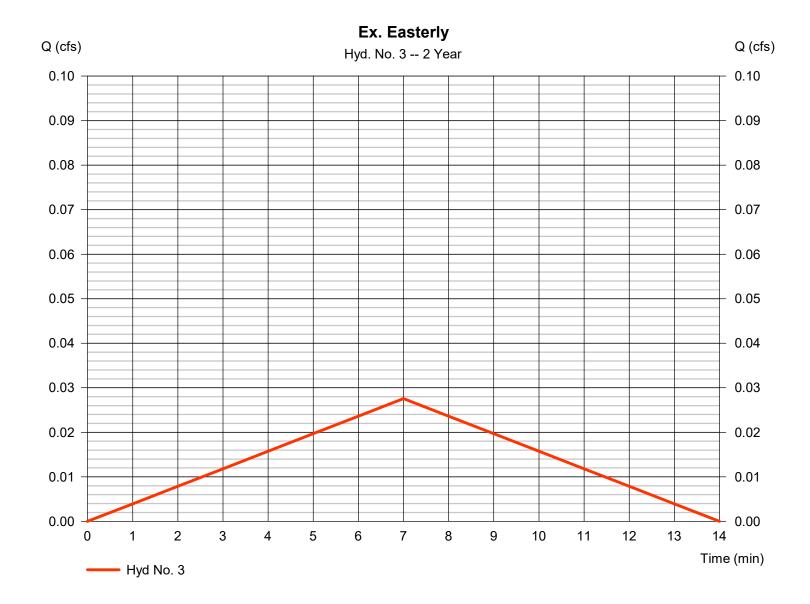
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

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Hyd. No. 3

Ex. Easterly

Hydrograph type = Rational Peak discharge = 0.028 cfsStorm frequency Time to peak = 2 yrs= 7 min Time interval = 1 min Hyd. volume = 12 cuft Drainage area Runoff coeff. = 0.080 ac= 0.1Tc by User $= 7.00 \, \text{min}$ Intensity = 3.445 in/hr= Railroad Street, Salisbury, CT ADSE/Renv/ein/hDFfact IDF Curve = 1/1



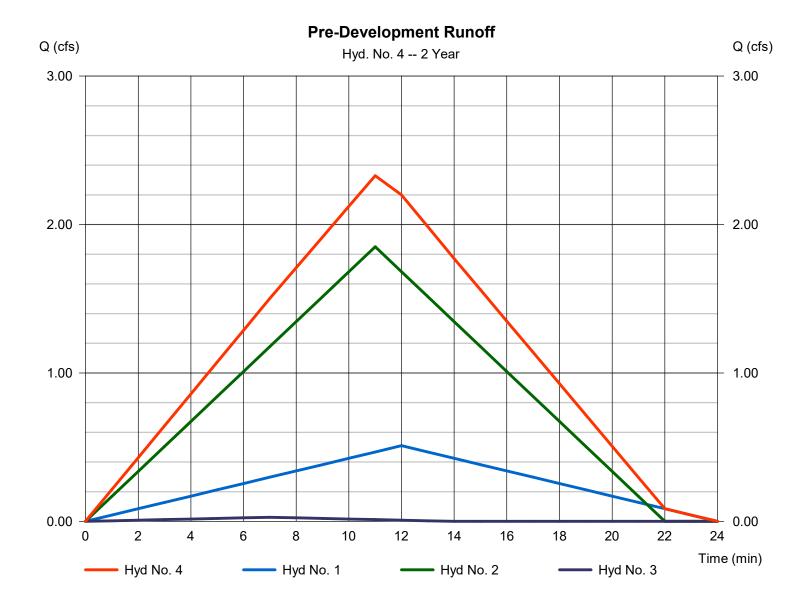
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

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Hyd. No. 4

Pre-Development Runoff

= 2.329 cfsHydrograph type = Combine Peak discharge Storm frequency Time to peak = 2 yrs= 11 min Time interval = 1 min Hyd. volume = 1,600 cuft Inflow hyds. = 1, 2, 3Contrib. drain. area = 6.250 ac



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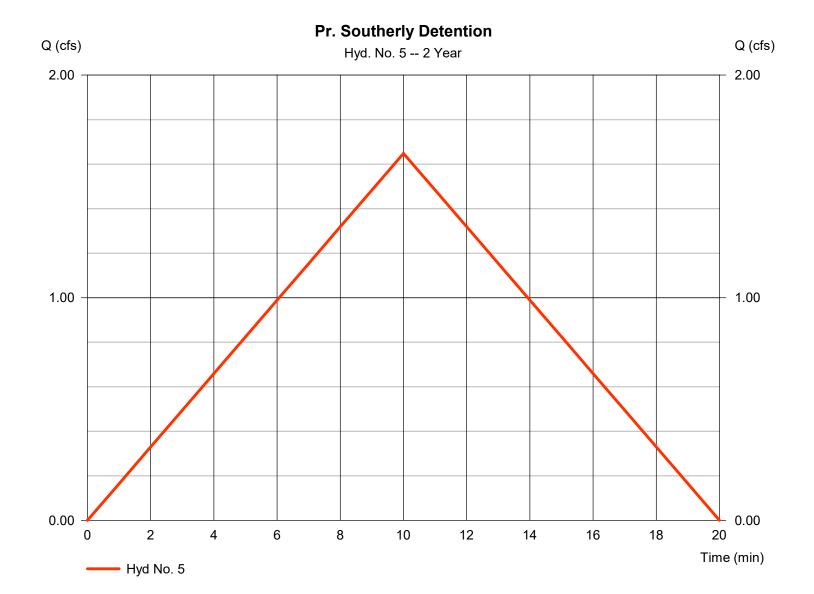
Monday, 11 / 20 / 2023

Hyd. No. 5

Pr. Southerly Detention

Hydrograph type = Rational Peak discharge = 1.648 cfsStorm frequency Time to peak = 2 yrs= 10 min Time interval = 1 min Hyd. volume = 989 cuft Drainage area = 1.330 ac Runoff coeff. = 0.43Tc by User $= 10.00 \, \text{min}$ Intensity = 2.882 in/hr

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Renovemb10 Fract = 1/1



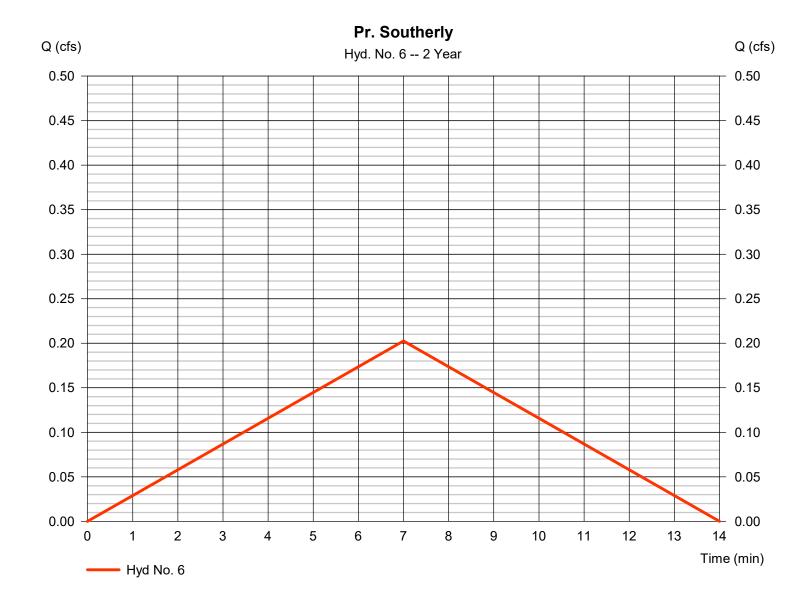
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

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Hyd. No. 6

Pr. Southerly

Hydrograph type = Rational Peak discharge = 0.203 cfsStorm frequency Time to peak = 2 yrs= 7 min Time interval = 1 min Hyd. volume = 85 cuft Drainage area Runoff coeff. = 0.490 ac= 0.12Tc by User $= 7.00 \, \text{min}$ Intensity = 3.445 in/hr= Railroad Street, Salisbury, CT ADSE/Renv/ein/hDFfact IDF Curve = 1/1



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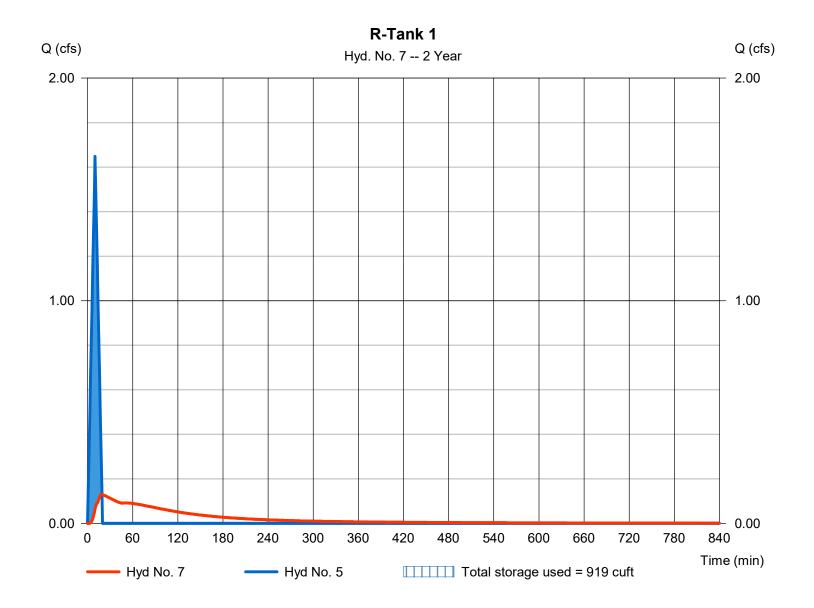
Monday, 11 / 20 / 2023

Hyd. No. 7

R-Tank 1

Hydrograph type = Reservoir Peak discharge = 0.130 cfsStorm frequency = 2 yrsTime to peak = 19 min Time interval = 1 min Hyd. volume = 941 cuft Inflow hyd. No. = 5 - Pr. Southerly Detention Max. Elevation $= 672.91 \, \text{ft}$ = Southerly Watershed R-Tank 1Max. Storage Reservoir name = 919 cuft

Storage Indication method used.



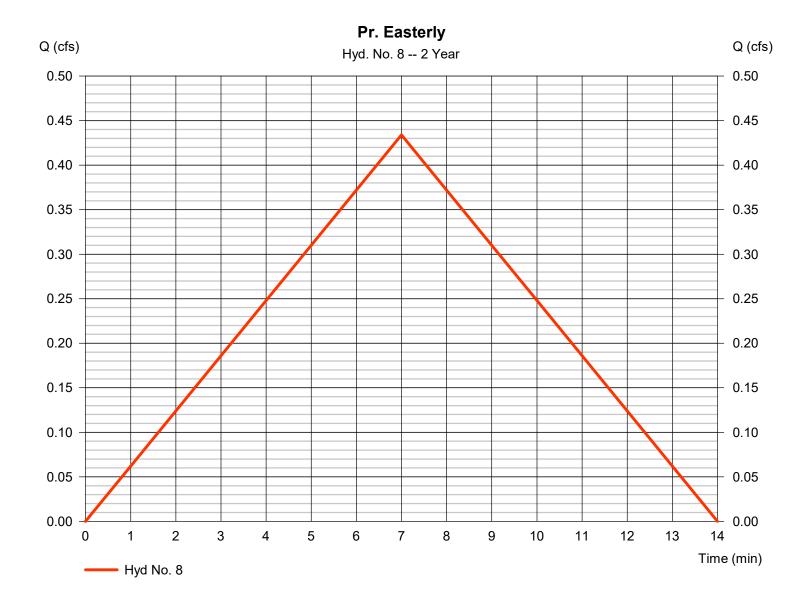
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Hyd. No. 8

Pr. Easterly

Hydrograph type = Rational Peak discharge = 0.434 cfsStorm frequency Time to peak = 2 yrs= 7 min Time interval = 1 min Hyd. volume = 182 cuft Drainage area Runoff coeff. = 0.300 ac= 0.42Tc by User $= 7.00 \, \text{min}$ Intensity = 3.445 in/hr= Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact IDF Curve = 1/1



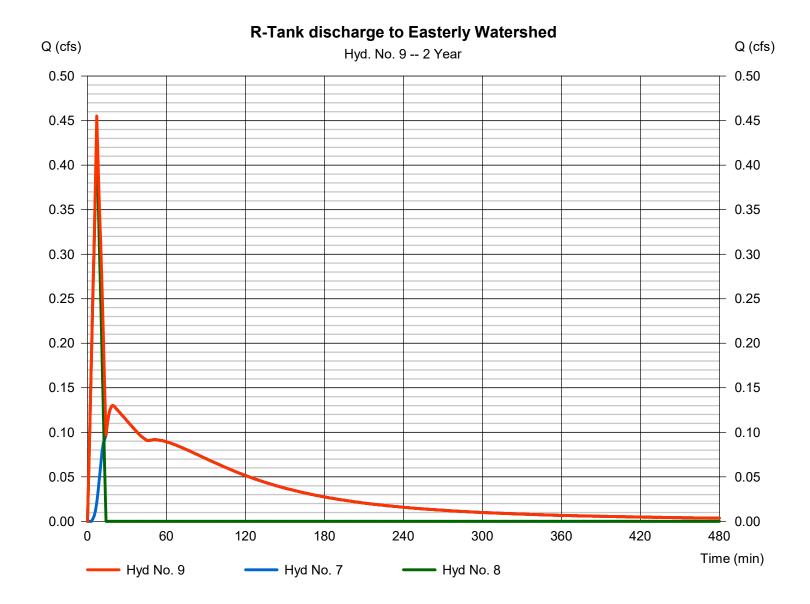
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Hyd. No. 9

R-Tank discharge to Easterly Watershed

Hydrograph type = Combine Peak discharge = 0.455 cfsStorm frequency Time to peak = 2 yrs= 7 min Time interval = 1 min Hyd. volume = 1,123 cuft Inflow hyds. = 7,8 Contrib. drain. area = 0.300 ac



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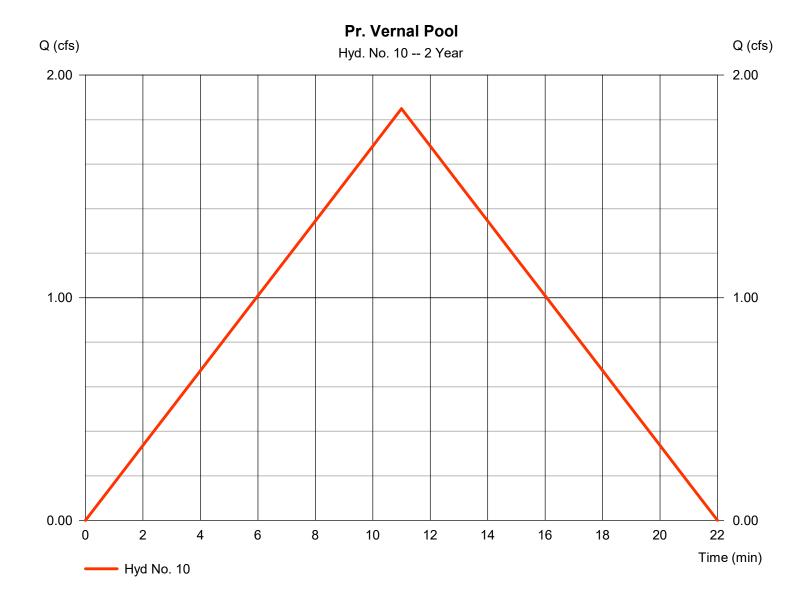
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Hyd. No. 10

Pr. Vernal Pool

Hydrograph type = Rational Peak discharge = 1.850 cfsStorm frequency = 2 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 1,221 cuft Drainage area = 3.750 acRunoff coeff. = 0.18Tc by User = 11.00 min Intensity = 2.740 in/hr

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Exerc/teinhDFfact = 1/1



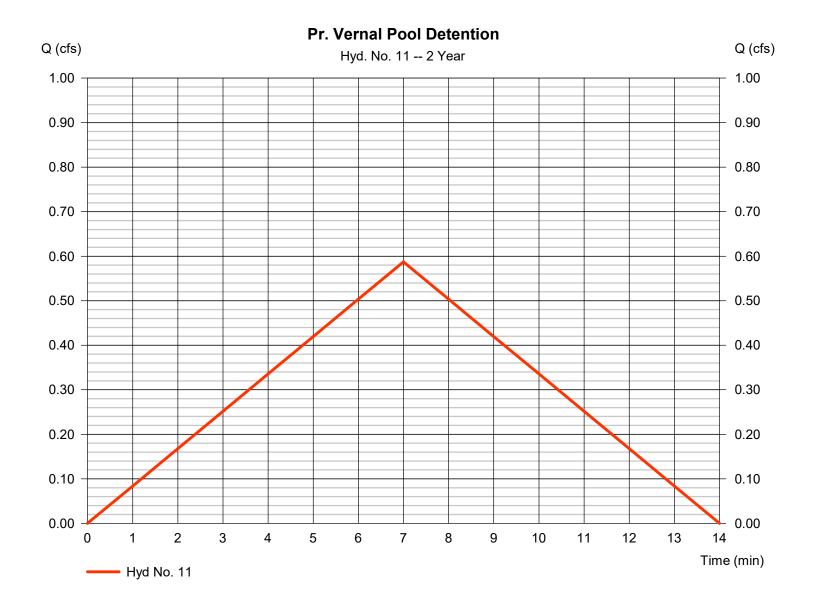
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Hyd. No. 11

Pr. Vernal Pool Detention

Hydrograph type Peak discharge = 0.587 cfs= Rational Storm frequency Time to peak = 2 yrs= 7 min Time interval = 1 min Hyd. volume = 247 cuft Drainage area Runoff coeff. = 0.550 ac= 0.31Tc by User Intensity = 3.445 in/hr $= 7.00 \, \text{min}$ = Railroad Street, Salisbury, CT ADSTE/Renc/BinhlDffact IDF Curve = 1/1



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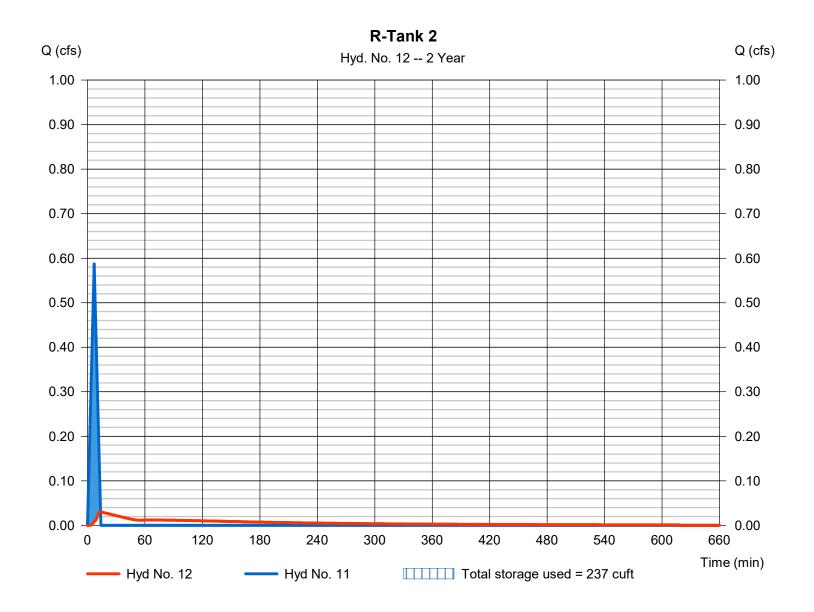
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Hyd. No. 12

R-Tank 2

Hydrograph type Peak discharge = 0.030 cfs= Reservoir Storm frequency Time to peak = 2 yrs= 14 min Time interval = 1 min Hyd. volume = 208 cuft Inflow hyd. No. = 11 - Pr. Vernal Pool Detention Max. Elevation $= 671.91 \, \text{ft}$ = Vernal Pool Watershed R-Tank/Pax. Storage Reservoir name = 237 cuft

Storage Indication method used.



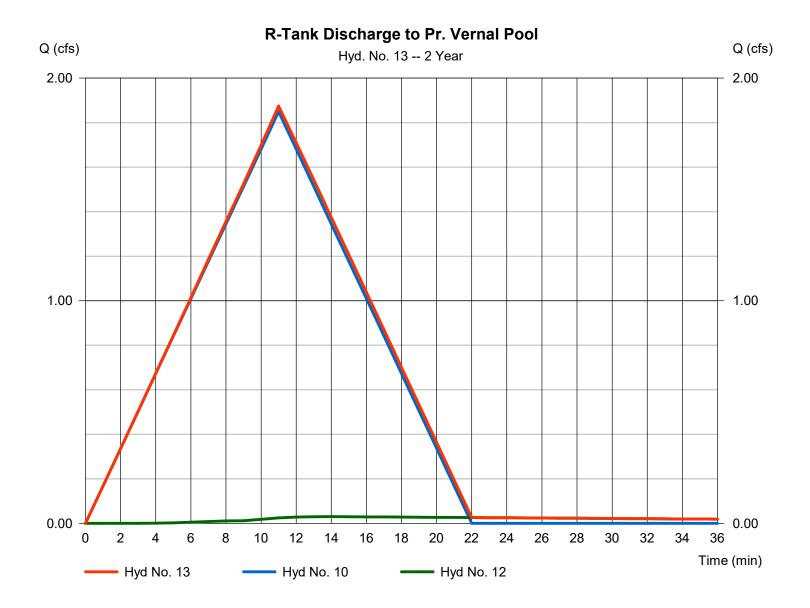
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Hyd. No. 13

R-Tank Discharge to Pr. Vernal Pool

Hydrograph type = Combine Peak discharge = 1.874 cfsStorm frequency Time to peak = 2 yrs= 11 min Time interval = 1 min Hyd. volume = 1,429 cuftInflow hyds. = 10, 12 Contrib. drain. area = 3.750 ac



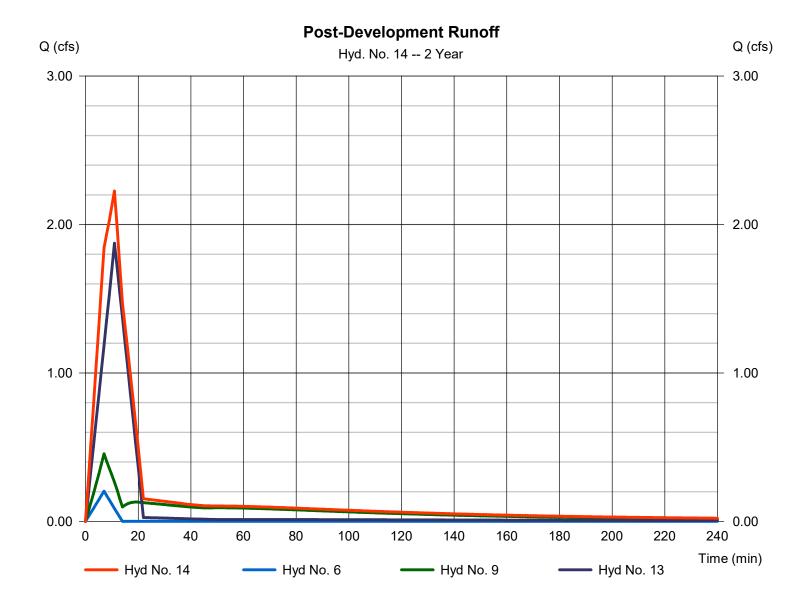
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Hyd. No. 14

Post-Development Runoff

= 2.225 cfsHydrograph type = Combine Peak discharge Storm frequency Time to peak = 2 yrs= 11 min Time interval = 1 min Hyd. volume = 2,637 cuftInflow hyds. = 6, 9, 13Contrib. drain. area = 0.490 ac



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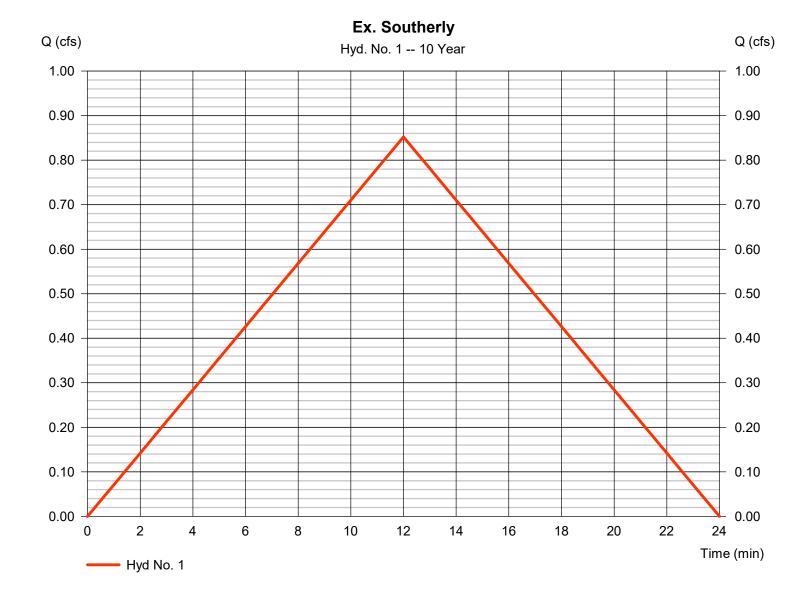
Hyd. No. 1

Ex. Southerly

Hydrograph type = Rational Peak discharge = 0.852 cfsStorm frequency Time to peak = 10 yrs= 12 min Time interval = 1 min Hyd. volume = 614 cuft Drainage area Runoff coeff. = 1.950 ac= 0.1

Intensity = 4.371 in/hr Tc by User = 12.00 min

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Renovemb10 Fract = 1/1



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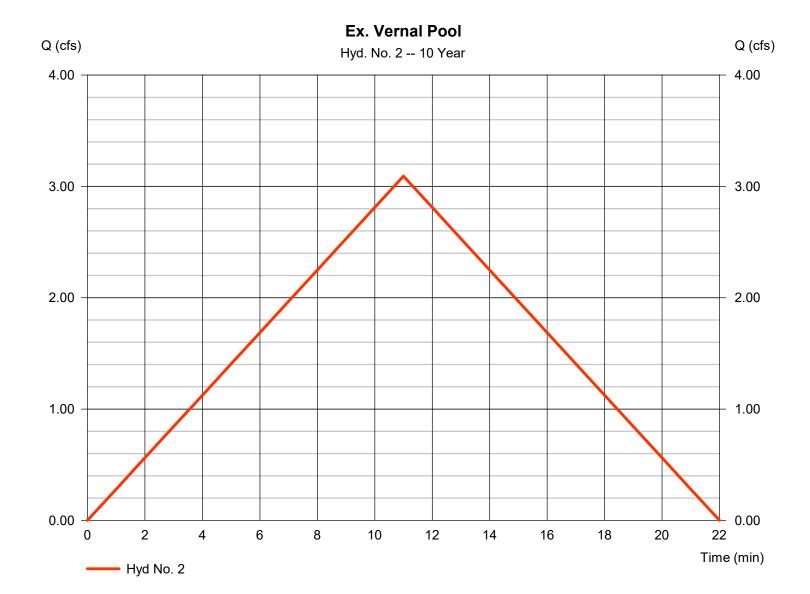
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Hyd. No. 2

Ex. Vernal Pool

Hydrograph type = Rational Peak discharge = 3.092 cfsStorm frequency = 10 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 2,041 cuftDrainage area = 4.220 acRunoff coeff. = 0.16Tc by User = 11.00 min Intensity = 4.580 in/hr

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Renovemb10 Fract = 1/1



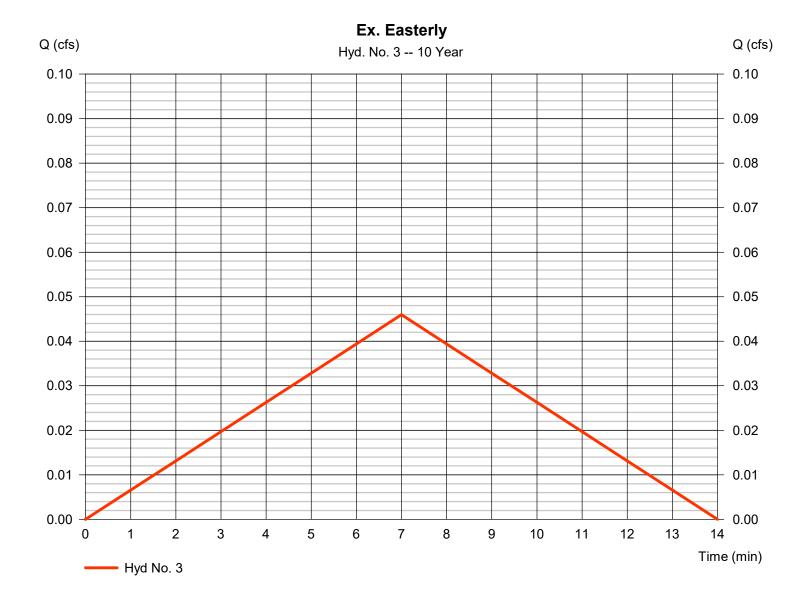
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Hyd. No. 3

Ex. Easterly

Hydrograph type = Rational Peak discharge = 0.046 cfsStorm frequency Time to peak = 10 yrs= 7 min Time interval = 1 min Hyd. volume = 19 cuft Drainage area Runoff coeff. = 0.080 ac= 0.1Tc by User $= 7.00 \, \text{min}$ Intensity = 5.745 in/hr= Railroad Street, Salisbury, CT ADSE/Renv/ein/hDFfact IDF Curve = 1/1



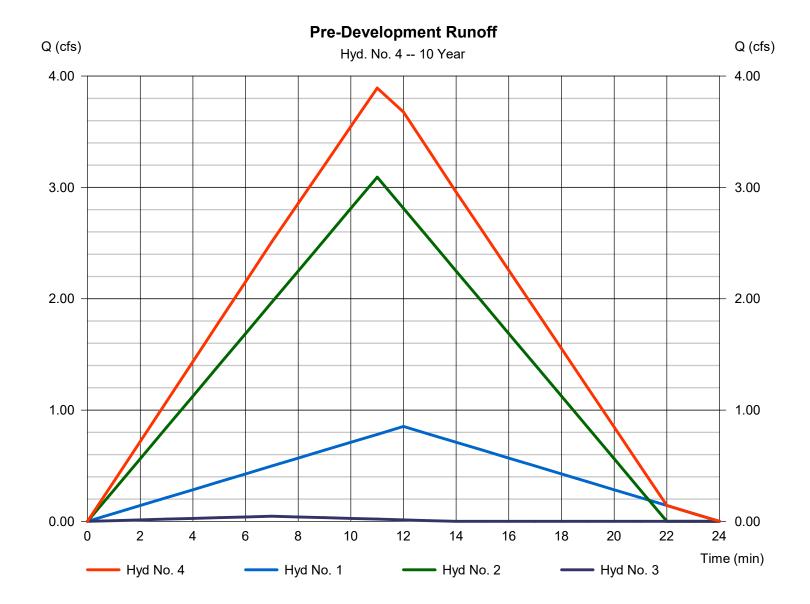
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Hyd. No. 4

Pre-Development Runoff

Hydrograph type = Combine Peak discharge = 3.893 cfsStorm frequency Time to peak = 10 yrs= 11 min Time interval = 1 min Hyd. volume = 2,674 cuftInflow hyds. = 1, 2, 3Contrib. drain. area = 6.250 ac



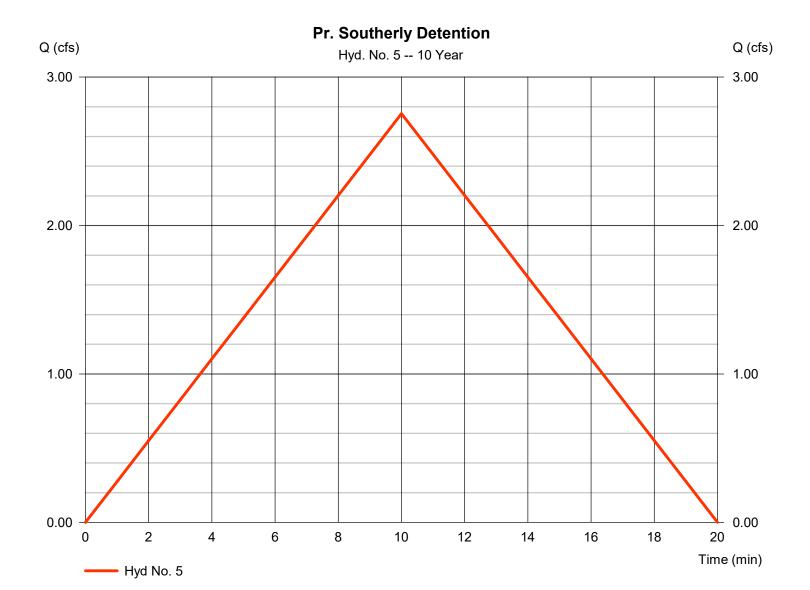
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Hyd. No. 5

Pr. Southerly Detention

= 2.754 cfsHydrograph type = Rational Peak discharge Storm frequency = 10 yrsTime to peak = 10 min Time interval = 1 min Hyd. volume = 1,652 cuft Drainage area Runoff coeff. = 1.330 ac= 0.43Tc by User $= 10.00 \, \text{min}$ Intensity = 4.815 in/hr= Railroad Street, Salisbury, CT ADSTE/Renc/BinhlDffact IDF Curve = 1/1



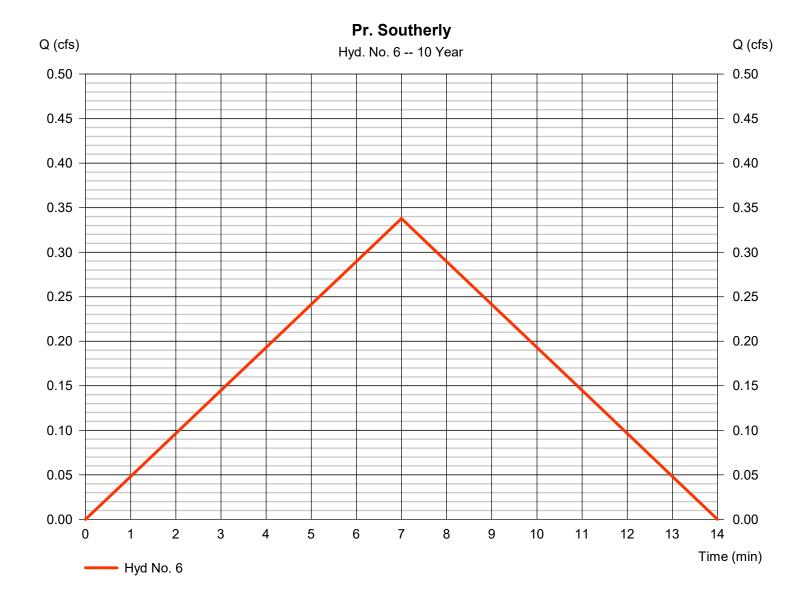
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Hyd. No. 6

Pr. Southerly

Hydrograph type = Rational Peak discharge = 0.338 cfsStorm frequency Time to peak = 10 yrs= 7 min Time interval = 1 min Hyd. volume = 142 cuft Drainage area Runoff coeff. = 0.490 ac= 0.12Tc by User $= 7.00 \, \text{min}$ Intensity = 5.745 in/hr= Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact IDF Curve = 1/1



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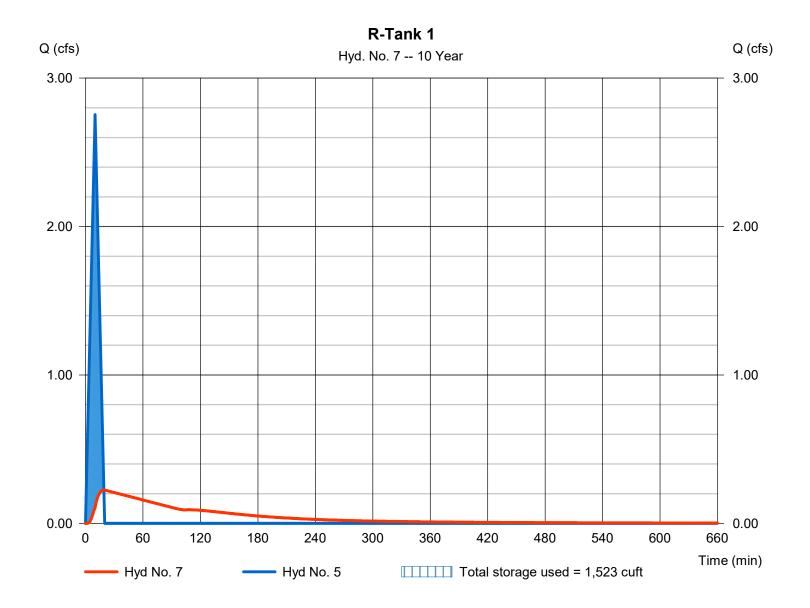
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Hyd. No. 7

R-Tank 1

Hydrograph type = Reservoir Peak discharge = 0.225 cfsStorm frequency = 10 yrsTime to peak = 19 min Time interval = 1 min Hyd. volume = 1,604 cuft Inflow hyd. No. = 5 - Pr. Southerly Detention Max. Elevation = 673.17 ft= Southerly Watershed R-Tank 1Max. Storage Reservoir name = 1,523 cuft

Storage Indication method used.



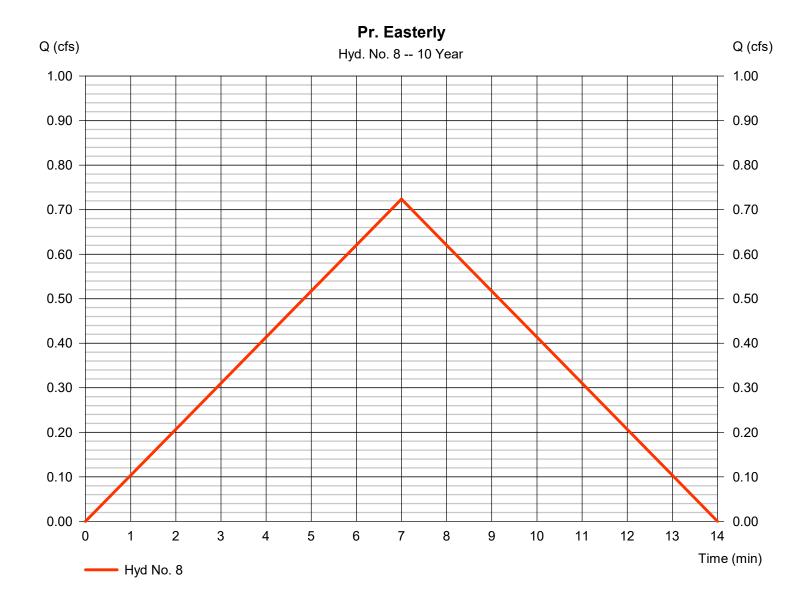
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Hyd. No. 8

Pr. Easterly

Hydrograph type = Rational Peak discharge = 0.724 cfsStorm frequency Time to peak = 10 yrs= 7 min Time interval = 1 min Hyd. volume = 304 cuft Drainage area Runoff coeff. = 0.300 ac= 0.42Tc by User $= 7.00 \, \text{min}$ Intensity = 5.745 in/hr= Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact IDF Curve = 1/1



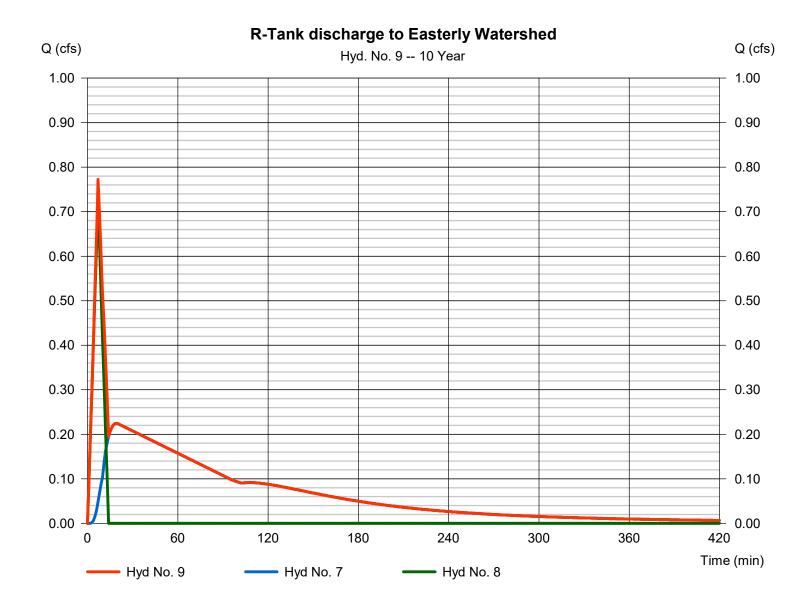
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Hyd. No. 9

R-Tank discharge to Easterly Watershed

Hydrograph type = Combine Peak discharge = 0.772 cfsStorm frequency = 10 yrsTime to peak = 7 min Time interval = 1 min Hyd. volume = 1,908 cuft Inflow hyds. = 7,8 Contrib. drain. area = 0.300 ac



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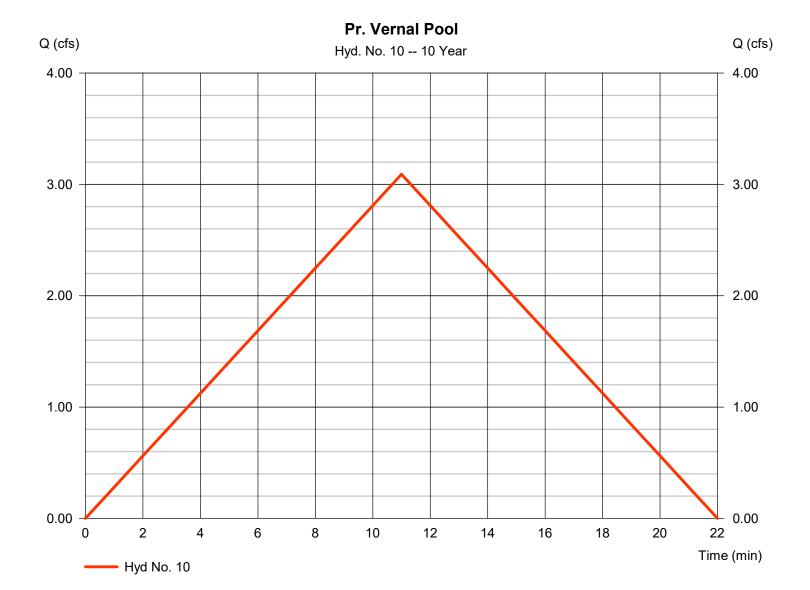
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Hyd. No. 10

Pr. Vernal Pool

Hydrograph type = Rational Peak discharge = 3.091 cfsStorm frequency = 10 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 2,040 cuftDrainage area Runoff coeff. = 3.750 ac= 0.18Tc by User = 11.00 min Intensity = 4.580 in/hr

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Renovemb10 Fract = 1/1



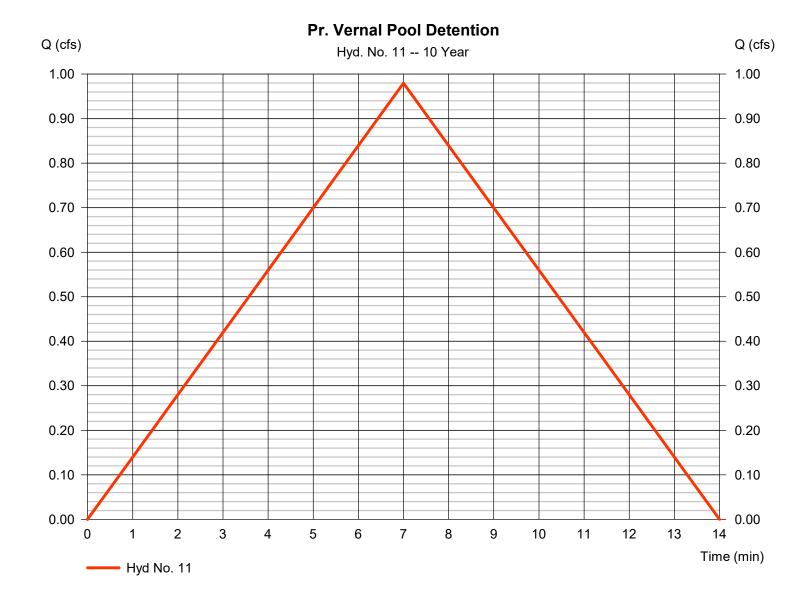
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Hyd. No. 11

Pr. Vernal Pool Detention

Hydrograph type Peak discharge = 0.980 cfs= Rational Storm frequency Time to peak = 10 yrs= 7 min Time interval = 1 min Hyd. volume = 411 cuft Drainage area Runoff coeff. = 0.550 ac= 0.31Tc by User Intensity = 5.745 in/hr $= 7.00 \, \text{min}$ = Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact IDF Curve = 1/1



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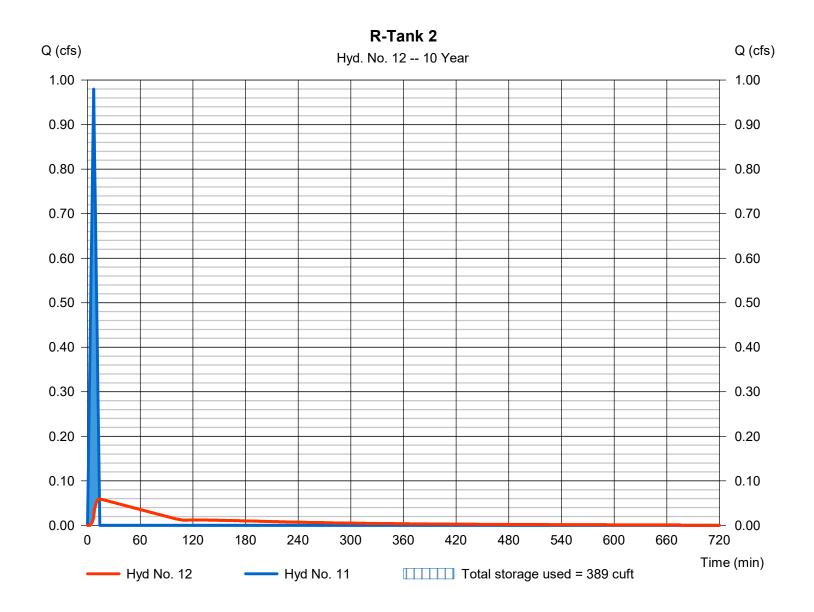
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Hyd. No. 12

R-Tank 2

Hydrograph type Peak discharge = 0.059 cfs= Reservoir Storm frequency Time to peak = 10 yrs= 14 min Time interval = 1 min Hyd. volume = 373 cuft Inflow hyd. No. = 11 - Pr. Vernal Pool Detention Max. Elevation = 672.18 ft= Vernal Pool Watershed R-Tank/Pax. Storage Reservoir name = 389 cuft

Storage Indication method used.



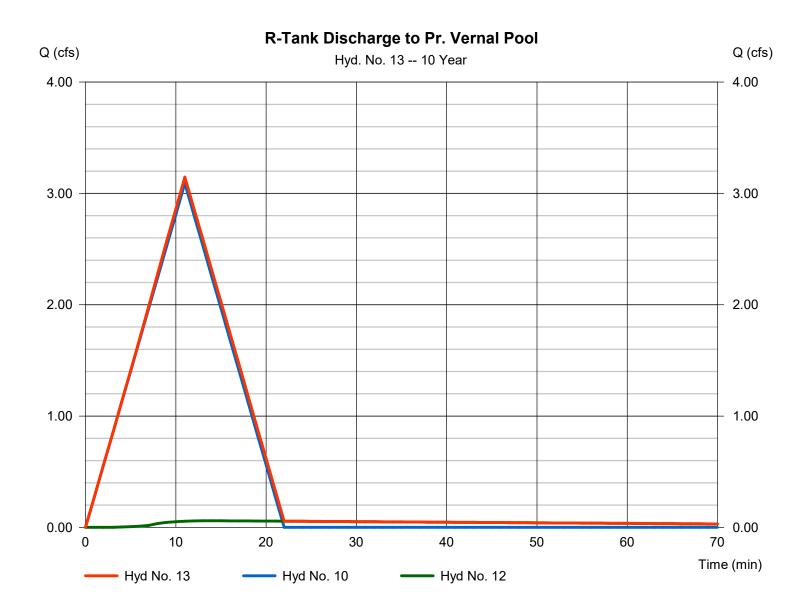
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Hyd. No. 13

R-Tank Discharge to Pr. Vernal Pool

Hydrograph type = Combine Peak discharge = 3.147 cfsStorm frequency Time to peak = 10 yrs= 11 min Time interval = 1 min Hyd. volume = 2,413 cuftInflow hyds. = 10, 12 Contrib. drain. area = 3.750 ac



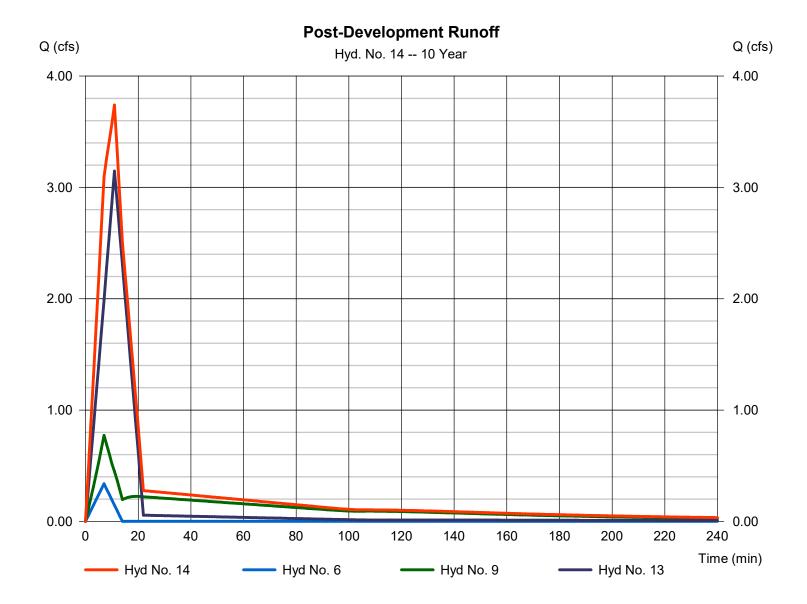
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Hyd. No. 14

Post-Development Runoff

Hydrograph type = Combine Peak discharge = 3.740 cfsStorm frequency Time to peak = 10 yrs= 11 min Time interval = 1 min Hyd. volume = 4,464 cuft Inflow hyds. Contrib. drain. area = 0.490 ac= 6, 9, 13



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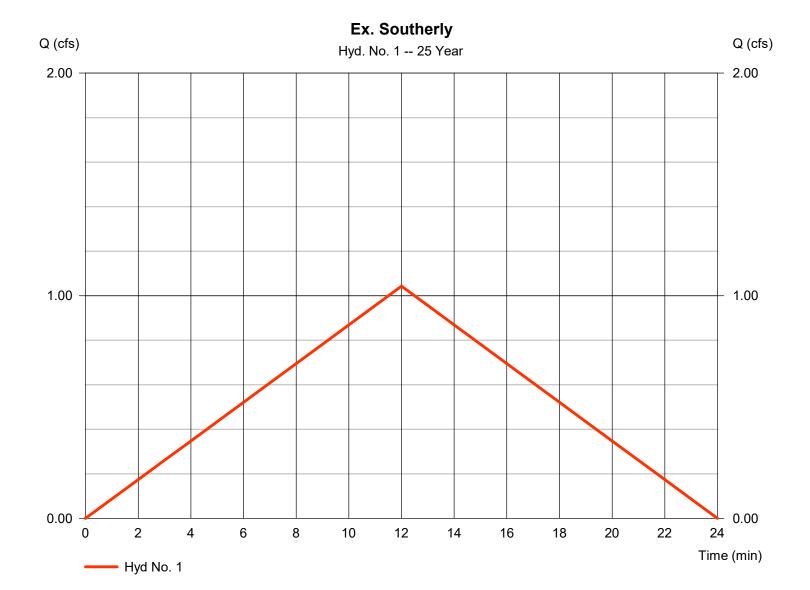
Hyd. No. 1

Ex. Southerly

Hydrograph type = Rational Peak discharge = 1.043 cfsStorm frequency = 25 yrsTime to peak = 12 min Time interval = 1 min Hyd. volume = 751 cuft Drainage area Runoff coeff. = 1.950 ac= 0.1

Intensity = 5.348 in/hr Tc by User = 12.00 min

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Exerc/teinhDFfact = 1/1



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

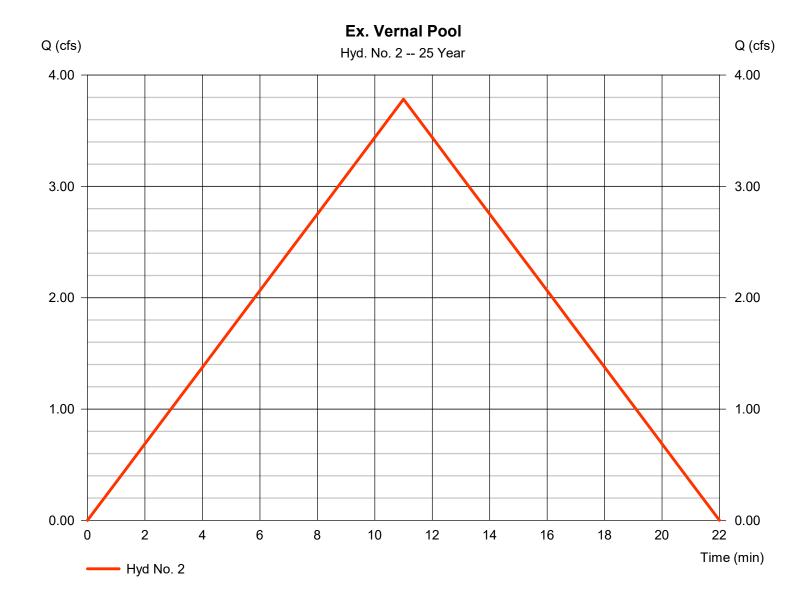
Monday, 11 / 20 / 2023

Hyd. No. 2

Ex. Vernal Pool

Hydrograph type = Rational Peak discharge = 3.784 cfsStorm frequency = 25 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 2,497 cuftDrainage area = 4.220 acRunoff coeff. = 0.16Tc by User = 11.00 min Intensity = 5.604 in/hr

IDF Curve = Railroad Street, Salisbury, CT ADSE/RenovenhDFact = 1/1



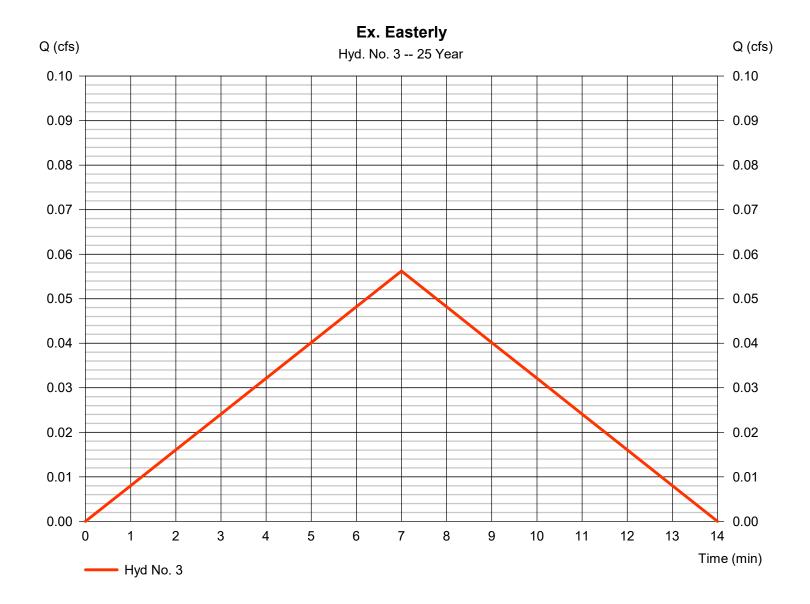
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Monday, 11 / 20 / 2023

Hyd. No. 3

Ex. Easterly

Hydrograph type = Rational Peak discharge = 0.056 cfsStorm frequency Time to peak = 25 yrs= 7 min Time interval = 1 min Hyd. volume = 24 cuft Drainage area Runoff coeff. = 0.1= 0.080 acTc by User $= 7.00 \, \text{min}$ Intensity = 7.028 in/hr= Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact IDF Curve = 1/1



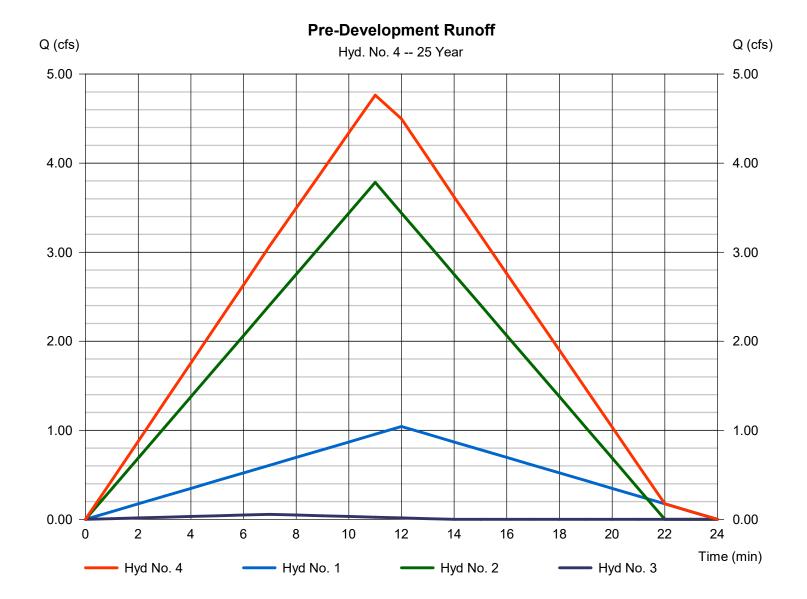
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Monday, 11 / 20 / 2023

Hyd. No. 4

Pre-Development Runoff

Hydrograph type = Combine Peak discharge = 4.764 cfsStorm frequency Time to peak = 25 yrs= 11 min = 3,272 cuft Time interval = 1 min Hyd. volume Inflow hyds. = 1, 2, 3Contrib. drain. area = 6.250 ac



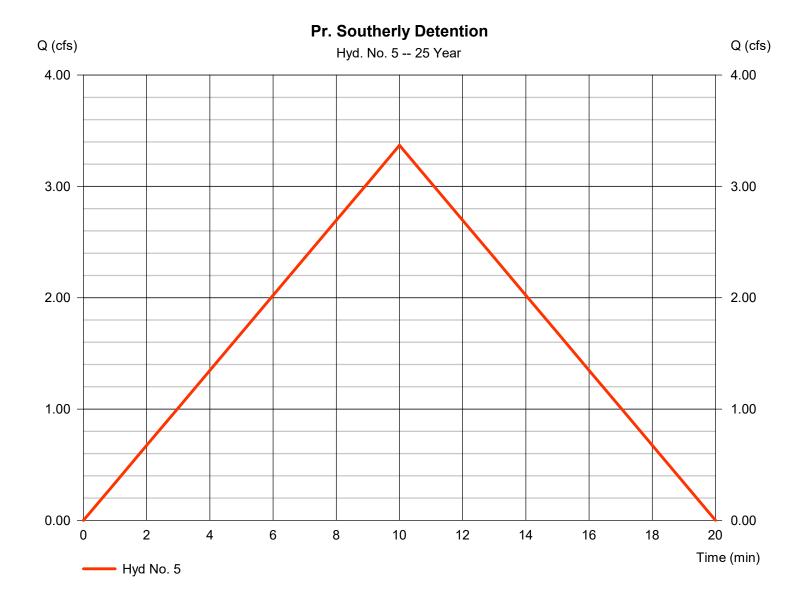
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Monday, 11 / 20 / 2023

Hyd. No. 5

Pr. Southerly Detention

Hydrograph type = Rational Peak discharge = 3.369 cfsStorm frequency = 25 yrsTime to peak = 10 min Time interval = 1 min Hyd. volume = 2,022 cuftDrainage area Runoff coeff. = 1.330 ac= 0.43Tc by User Intensity = 5.891 in/hr $= 10.00 \, \text{min}$ = Railroad Street, Salisbury, CT ADSTE/Renc/BinhlDffact IDF Curve = 1/1



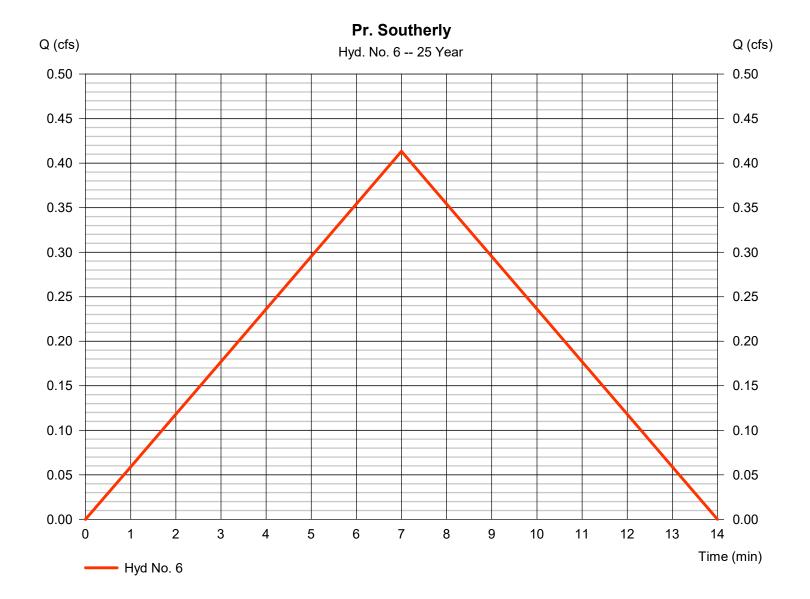
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Monday, 11 / 20 / 2023

Hyd. No. 6

Pr. Southerly

Hydrograph type = Rational Peak discharge = 0.413 cfsStorm frequency = 25 yrsTime to peak = 7 min Time interval = 1 min Hyd. volume = 174 cuft Runoff coeff. Drainage area = 0.490 ac= 0.12Tc by User $= 7.00 \, \text{min}$ Intensity = 7.028 in/hr= Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact IDF Curve = 1/1



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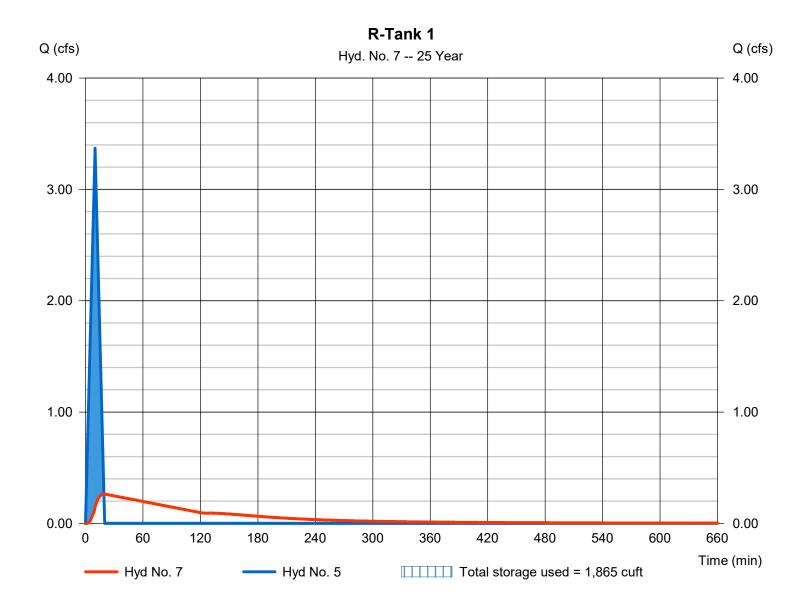
Monday, 11 / 20 / 2023

Hyd. No. 7

R-Tank 1

Hydrograph type Peak discharge = 0.264 cfs= Reservoir Storm frequency = 25 yrsTime to peak = 19 min Time interval = 1 min Hyd. volume = 1,974 cuft Max. Elevation Inflow hyd. No. = 5 - Pr. Southerly Detention = 673.32 ft= Southerly Watershed R-Tank 1Max. Storage Reservoir name = 1,865 cuft

Storage Indication method used.



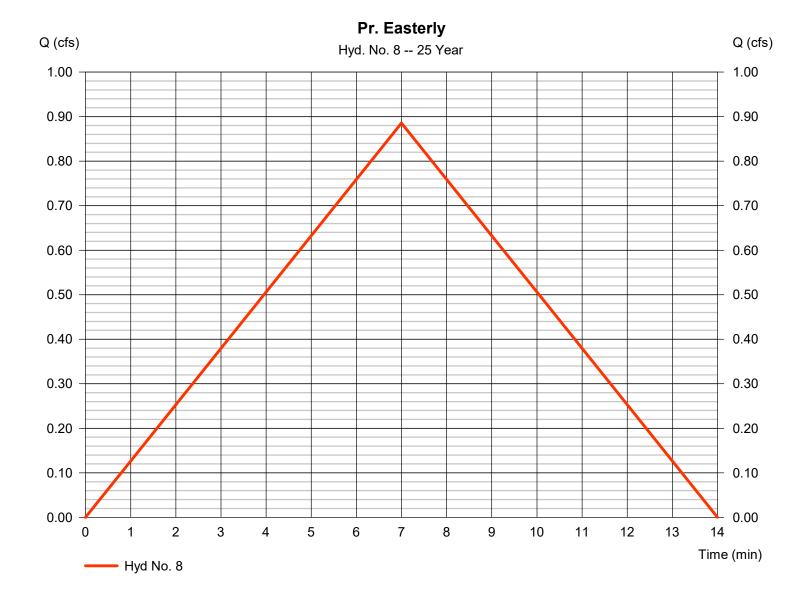
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Monday, 11 / 20 / 2023

Hyd. No. 8

Pr. Easterly

Hydrograph type = Rational Peak discharge = 0.886 cfsStorm frequency = 25 yrsTime to peak = 7 min Time interval = 1 min Hyd. volume = 372 cuft Runoff coeff. Drainage area = 0.300 ac= 0.42Tc by User $= 7.00 \, \text{min}$ Intensity = 7.028 in/hr= Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact IDF Curve = 1/1



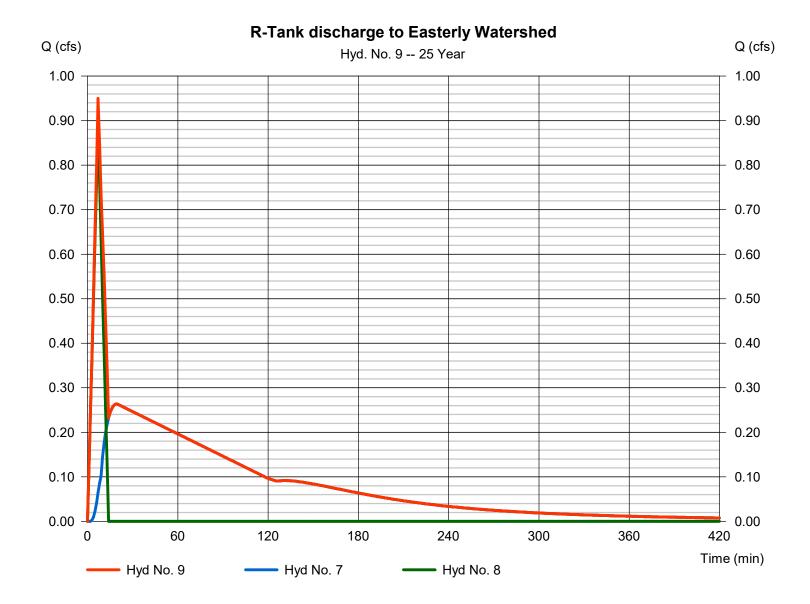
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Monday, 11 / 20 / 2023

Hyd. No. 9

R-Tank discharge to Easterly Watershed

Hydrograph type = Combine Peak discharge = 0.950 cfsStorm frequency Time to peak = 25 yrs= 7 min Time interval = 1 min Hyd. volume = 2,345 cuftInflow hyds. = 7,8 Contrib. drain. area = 0.300 ac



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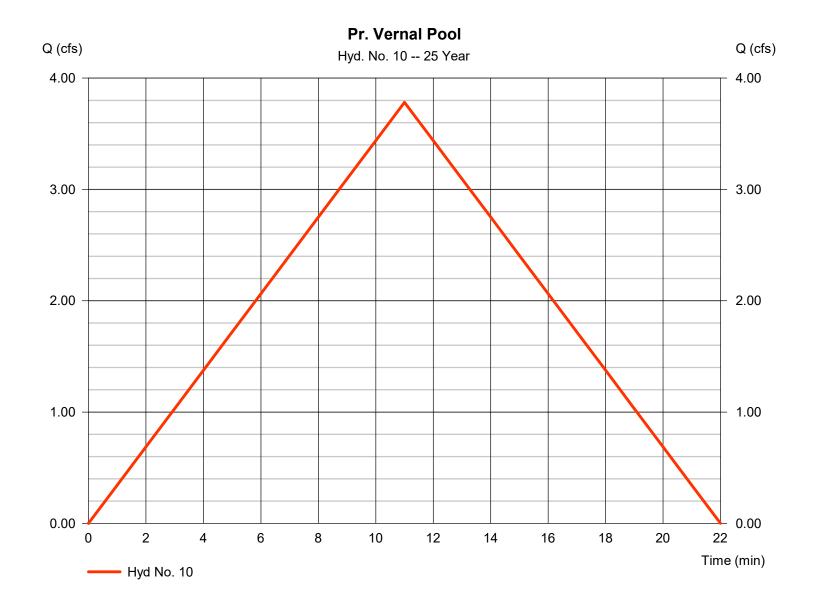
Monday, 11 / 20 / 2023

Hyd. No. 10

Pr. Vernal Pool

Hydrograph type = Rational Peak discharge = 3.782 cfsStorm frequency = 25 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 2,496 cuftDrainage area Runoff coeff. = 3.750 ac= 0.18Tc by User = 11.00 min Intensity = 5.604 in/hr

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Renovemb10 Fact = 1/1



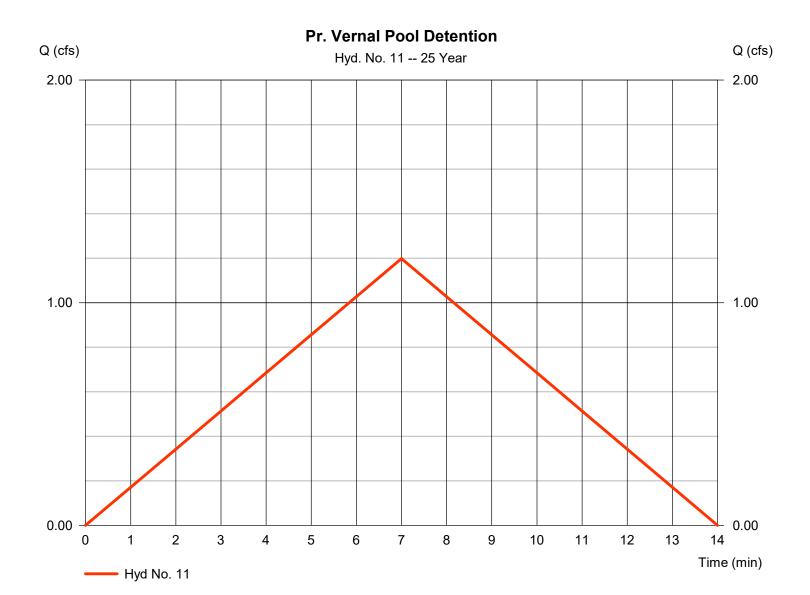
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Monday, 11 / 20 / 2023

Hyd. No. 11

Pr. Vernal Pool Detention

= 1.198 cfsHydrograph type = Rational Peak discharge Storm frequency = 7 min = 25 yrsTime to peak Time interval = 1 min Hyd. volume = 503 cuft Drainage area Runoff coeff. = 0.31= 0.550 acTc by User $= 7.00 \, \text{min}$ Intensity = 7.028 in/hr= Railroad Street, Salisbury, CT ADSTE/Renovember IDF Curve = 1/1



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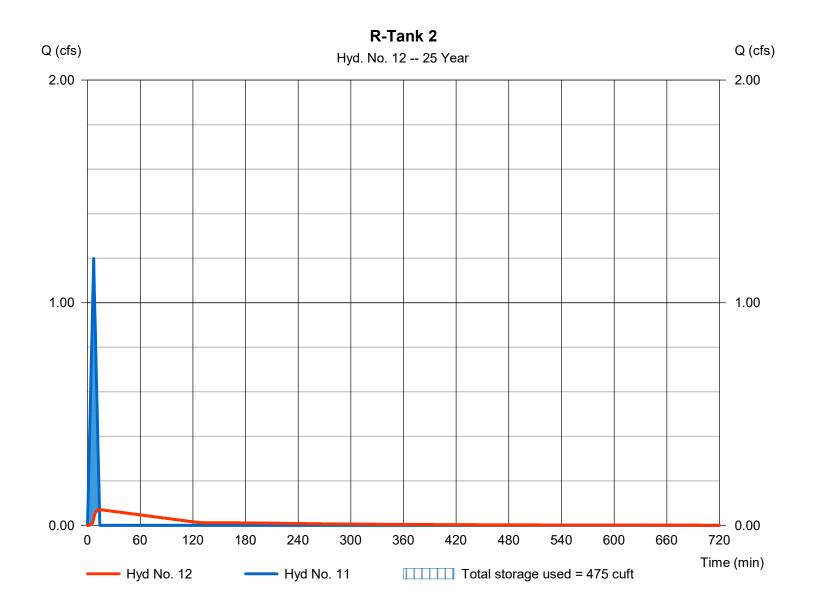
Monday, 11 / 20 / 2023

Hyd. No. 12

R-Tank 2

Hydrograph type = Reservoir Peak discharge = 0.071 cfsStorm frequency = 25 yrsTime to peak = 14 min Time interval = 1 min Hyd. volume = 465 cuft Inflow hyd. No. = 11 - Pr. Vernal Pool Detention Max. Elevation = 672.33 ft= Vernal Pool Watershed R-Tank/Pax. Storage Reservoir name = 475 cuft

Storage Indication method used.



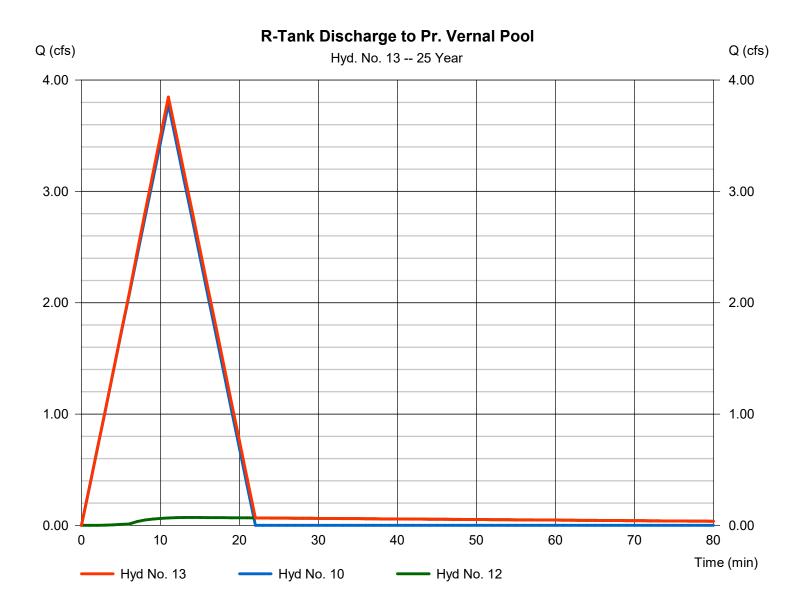
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Monday, 11 / 20 / 2023

Hyd. No. 13

R-Tank Discharge to Pr. Vernal Pool

Hydrograph type = Combine Peak discharge = 3.849 cfsStorm frequency Time to peak = 25 yrs= 11 min Time interval = 1 min Hyd. volume = 2,961 cuftInflow hyds. = 10, 12 Contrib. drain. area = 3.750 ac



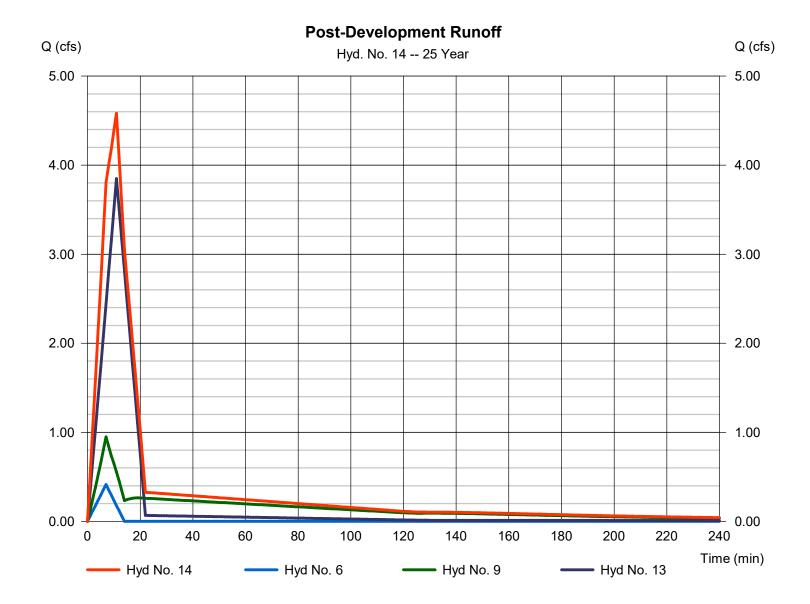
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Monday, 11 / 20 / 2023

Hyd. No. 14

Post-Development Runoff

Hydrograph type = Combine Peak discharge = 4.581 cfsStorm frequency Time to peak = 25 yrs= 11 min Time interval = 1 min Hyd. volume = 5,480 cuftInflow hyds. = 6, 9, 13Contrib. drain. area = 0.490 ac



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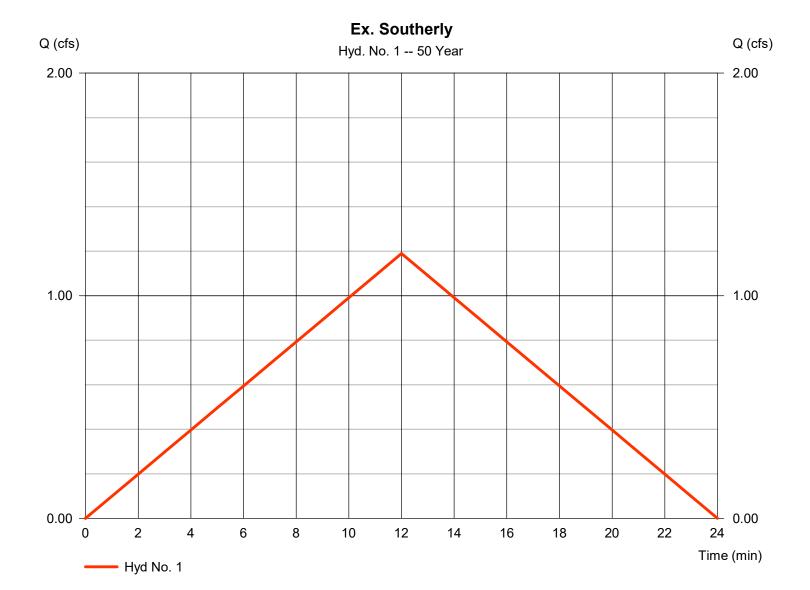
Hyd. No. 1

Ex. Southerly

Hydrograph type = Rational Peak discharge = 1.190 cfsStorm frequency = 50 yrsTime to peak = 12 min Time interval = 1 min Hyd. volume = 857 cuft Drainage area Runoff coeff. = 1.950 ac= 0.1

Intensity = 6.101 in/hr Tc by User = 12.00 min

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Exerc/teinhDFfact = 1/1



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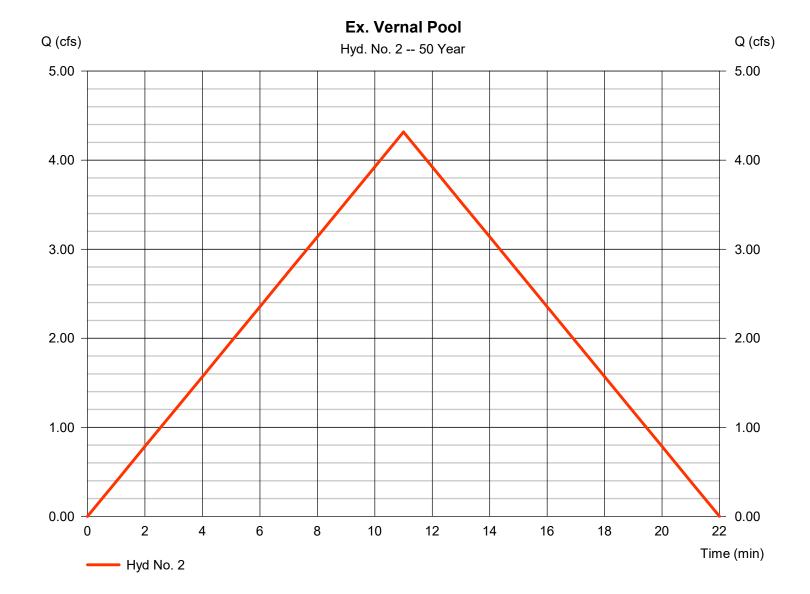
Monday, 11 / 20 / 2023

Hyd. No. 2

Ex. Vernal Pool

Hydrograph type = Rational Peak discharge = 4.316 cfsStorm frequency = 50 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 2,849 cuftDrainage area Runoff coeff. = 4.220 ac= 0.16Tc by User = 11.00 min Intensity = 6.393 in/hr

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Renovemb10 Fract = 1/1



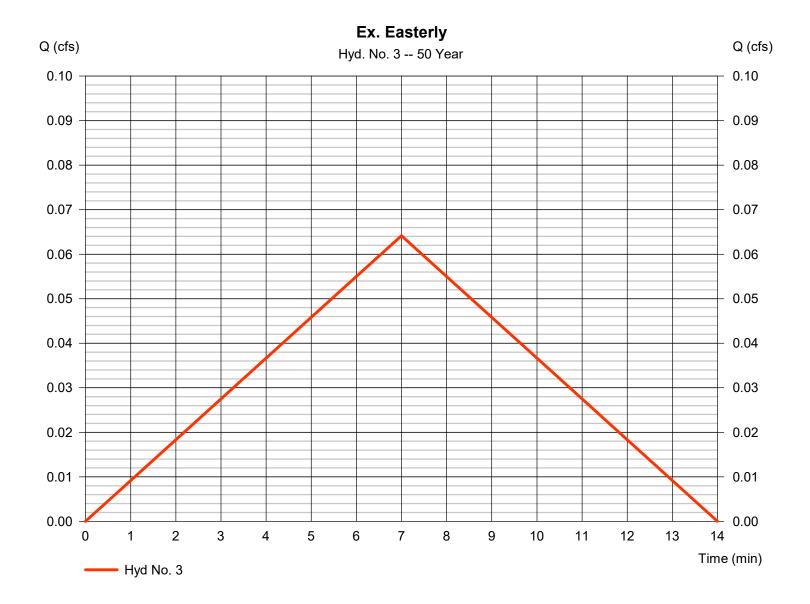
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Monday, 11 / 20 / 2023

Hyd. No. 3

Ex. Easterly

Hydrograph type = Rational Peak discharge = 0.064 cfsStorm frequency Time to peak = 50 yrs= 7 min Time interval = 1 min Hyd. volume = 27 cuft Drainage area Runoff coeff. = 0.080 ac= 0.1Tc by User $= 7.00 \, \text{min}$ Intensity = 8.017 in/hr= Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact IDF Curve = 1/1



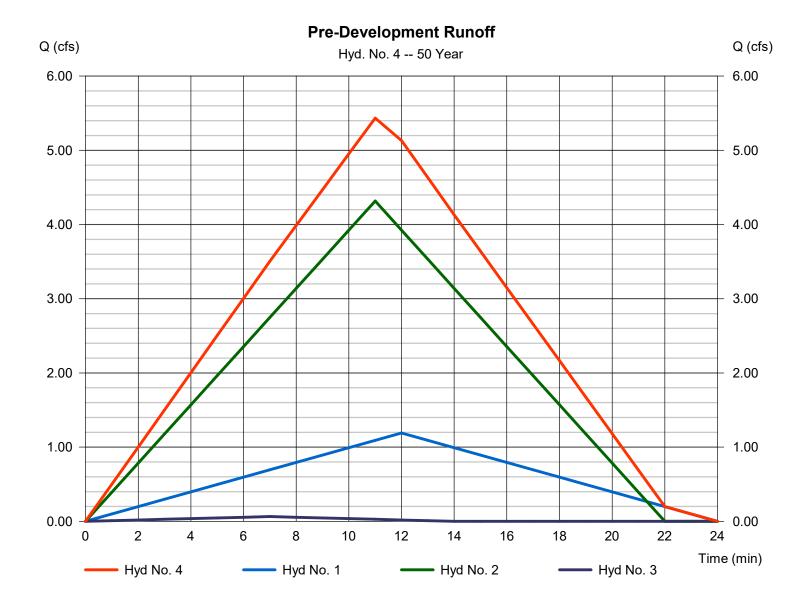
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Monday, 11 / 20 / 2023

Hyd. No. 4

Pre-Development Runoff

Hydrograph type = Combine Peak discharge = 5.435 cfsStorm frequency = 50 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 3,732 cuftInflow hyds. = 1, 2, 3Contrib. drain. area = 6.250 ac



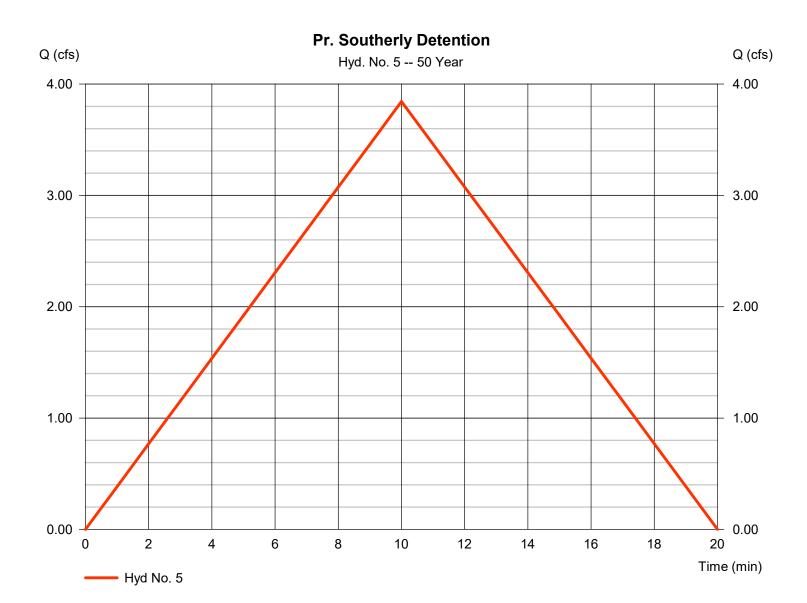
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Monday, 11 / 20 / 2023

Hyd. No. 5

Pr. Southerly Detention

Hydrograph type = Rational Peak discharge = 3.844 cfsStorm frequency Time to peak = 50 yrs= 10 min Time interval = 1 min Hyd. volume = 2,306 cuftDrainage area Runoff coeff. = 1.330 ac= 0.43Tc by User Intensity = 6.721 in/hr $= 10.00 \, \text{min}$ = Railroad Street, Salisbury, CT ADSTE/Renc/BinhlDffact IDF Curve = 1/1



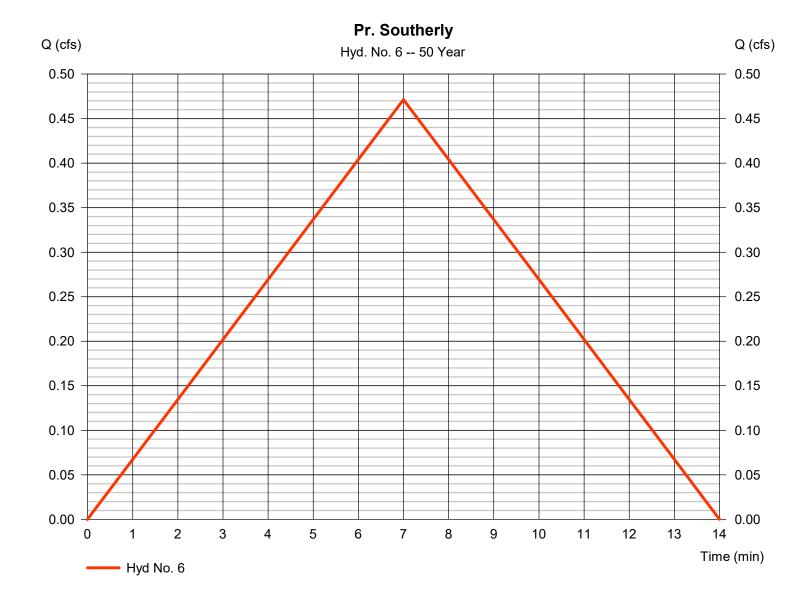
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Monday, 11 / 20 / 2023

Hyd. No. 6

Pr. Southerly

Hydrograph type = Rational Peak discharge = 0.471 cfsStorm frequency = 50 yrsTime to peak = 7 min Time interval = 1 min Hyd. volume = 198 cuft Drainage area Runoff coeff. = 0.490 ac= 0.12Tc by User $= 7.00 \, \text{min}$ Intensity = 8.017 in/hr= Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact IDF Curve = 1/1



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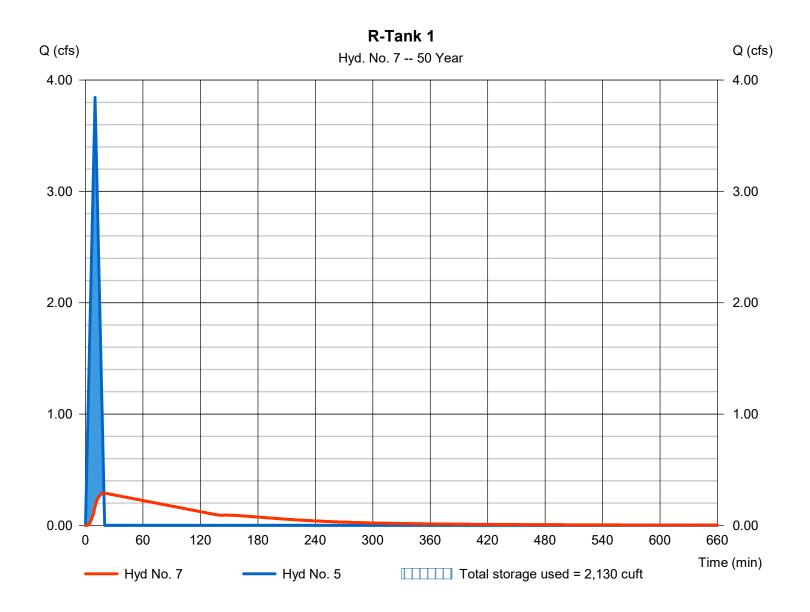
Monday, 11 / 20 / 2023

Hyd. No. 7

R-Tank 1

Hydrograph type Peak discharge = 0.290 cfs= Reservoir Storm frequency = 50 yrsTime to peak = 19 min Time interval = 1 min Hyd. volume = 2,258 cuftMax. Elevation Inflow hyd. No. = 5 - Pr. Southerly Detention = 673.44 ft= Southerly Watershed R-Tank 1Max. Storage Reservoir name = 2,130 cuft

Storage Indication method used.



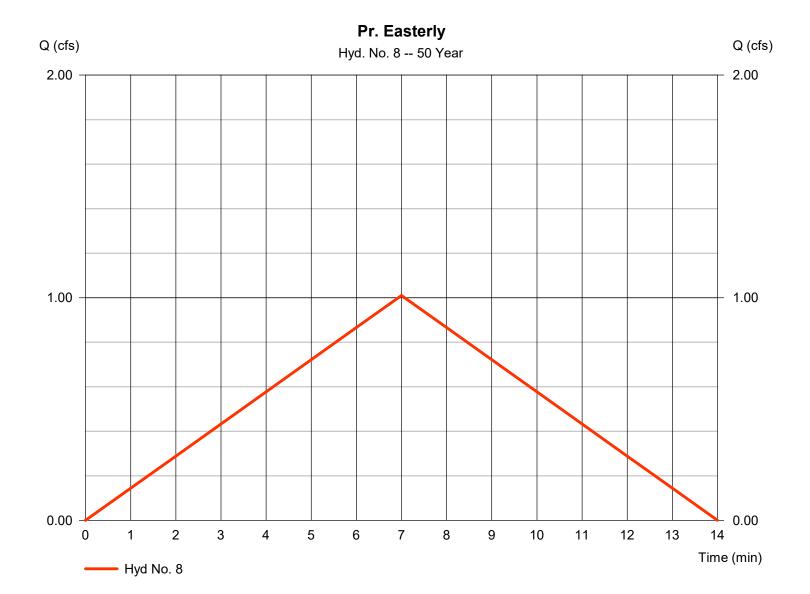
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Monday, 11 / 20 / 2023

Hyd. No. 8

Pr. Easterly

Hydrograph type = 1.010 cfs= Rational Peak discharge Storm frequency = 50 yrsTime to peak = 7 min Time interval = 1 min Hyd. volume = 424 cuft Drainage area = 0.42Runoff coeff. = 0.300 acTc by User $= 7.00 \, \text{min}$ Intensity = 8.017 in/hr= Railroad Street, Salisbury, CT ADSE/Renovembn Fact IDF Curve = 1/1



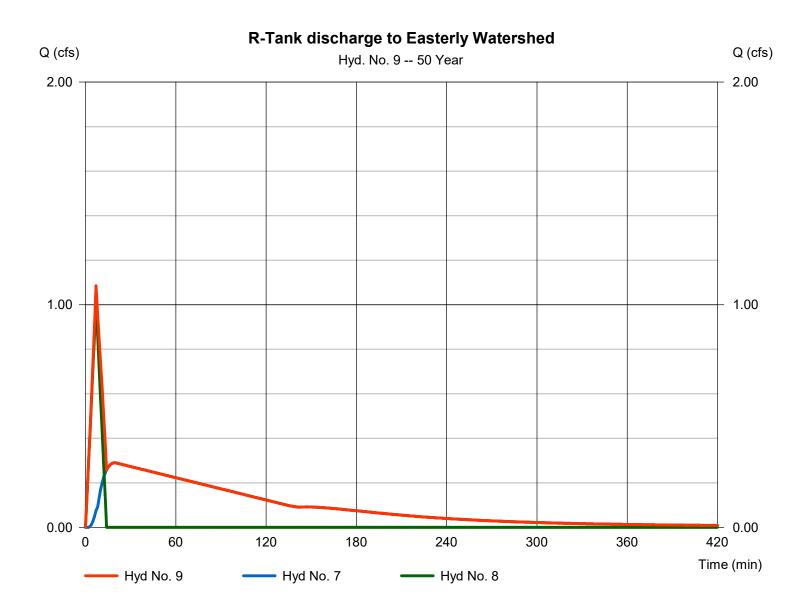
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Monday, 11 / 20 / 2023

Hyd. No. 9

R-Tank discharge to Easterly Watershed

Hydrograph type = Combine Peak discharge = 1.086 cfsStorm frequency = 50 yrsTime to peak = 7 min Time interval = 1 min Hyd. volume = 2,683 cuftInflow hyds. = 7,8 Contrib. drain. area = 0.300 ac



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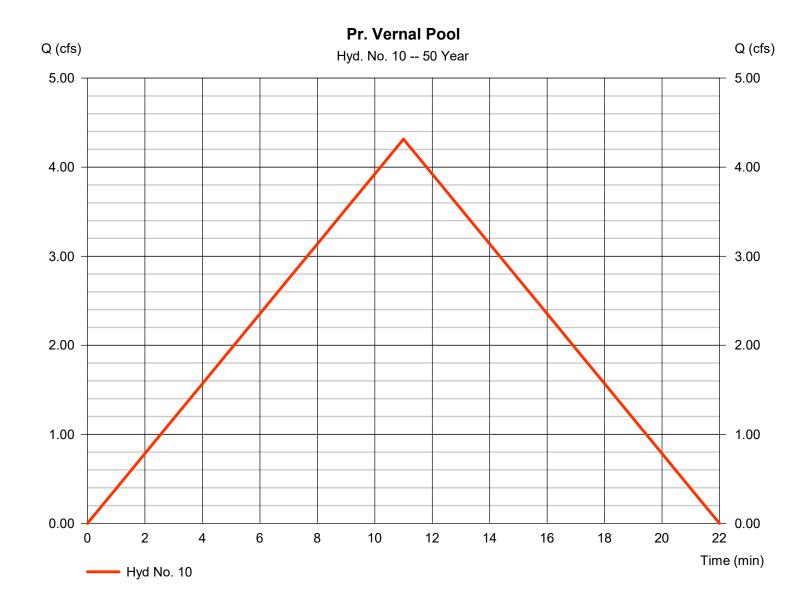
Monday, 11 / 20 / 2023

Hyd. No. 10

Pr. Vernal Pool

Hydrograph type = Rational Peak discharge = 4.315 cfsStorm frequency = 50 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 2,848 cuft Drainage area Runoff coeff. = 3.750 ac= 0.18Tc by User = 11.00 min Intensity = 6.393 in/hr

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Renovemb10 Fact = 1/1



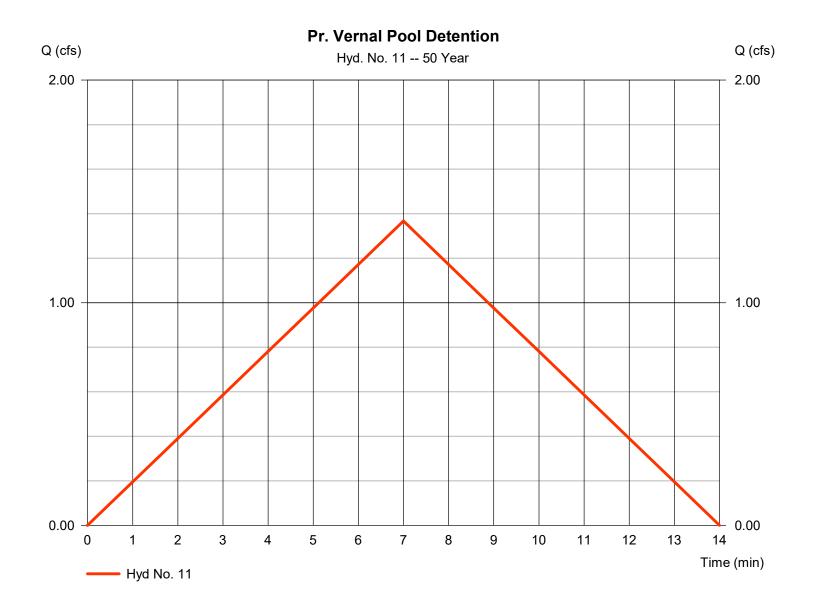
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Monday, 11 / 20 / 2023

Hyd. No. 11

Pr. Vernal Pool Detention

= 1.367 cfsHydrograph type = Rational Peak discharge Storm frequency = 50 yrsTime to peak = 7 min Time interval = 1 min Hyd. volume = 574 cuft Drainage area Runoff coeff. = 0.31= 0.550 acTc by User $= 7.00 \, \text{min}$ Intensity = 8.017 in/hr= Railroad Street, Salisbury, CT ADSTE/Renovember IDF Curve = 1/1



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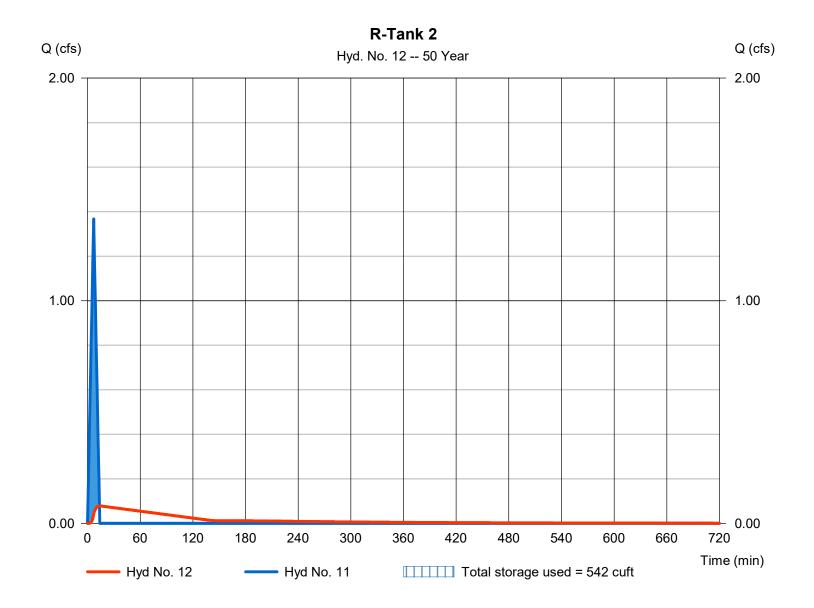
Monday, 11 / 20 / 2023

Hyd. No. 12

R-Tank 2

Hydrograph type = Reservoir Peak discharge = 0.079 cfsStorm frequency = 50 yrsTime to peak = 14 min Time interval = 1 min Hyd. volume = 536 cuft Inflow hyd. No. = 11 - Pr. Vernal Pool Detention Max. Elevation = 672.44 ft= Vernal Pool Watershed R-Tank/Pax. Storage Reservoir name = 542 cuft

Storage Indication method used.



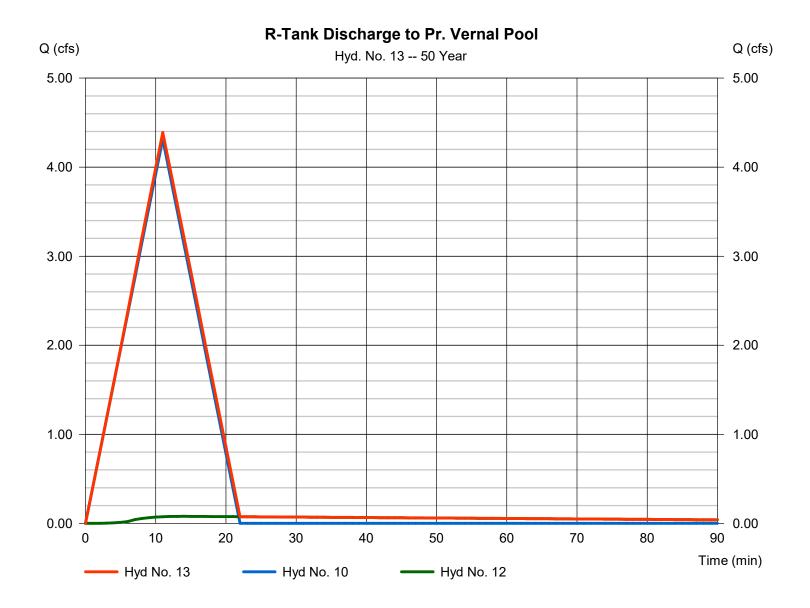
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Hyd. No. 13

R-Tank Discharge to Pr. Vernal Pool

Hydrograph type = Combine Peak discharge = 4.389 cfsStorm frequency Time to peak = 50 yrs= 11 min Time interval = 1 min Hyd. volume = 3,384 cuft Inflow hyds. = 10, 12 Contrib. drain. area = 3.750 ac



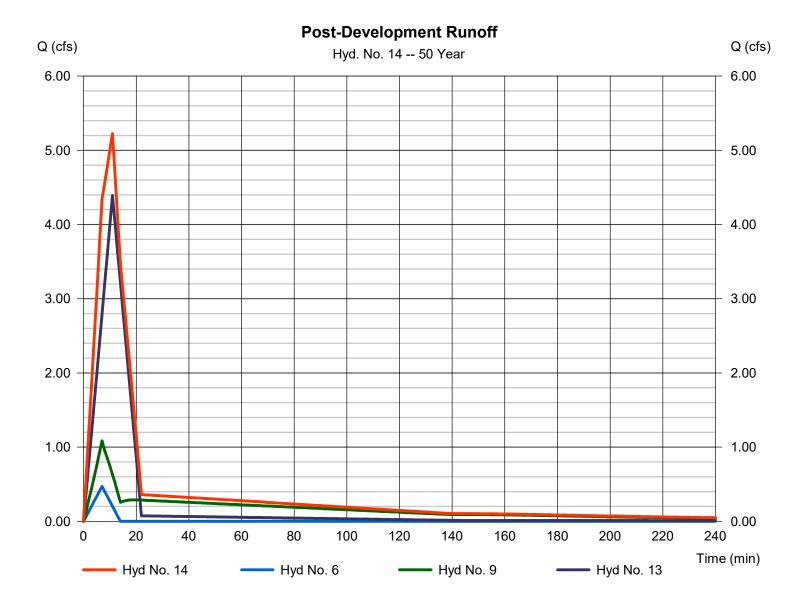
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Hyd. No. 14

Post-Development Runoff

Hydrograph type = Combine Peak discharge = 5.224 cfsStorm frequency Time to peak = 50 yrs= 11 min Time interval = 1 min Hyd. volume = 6,264 cuft Inflow hyds. Contrib. drain. area = 6, 9, 13= 0.490 ac



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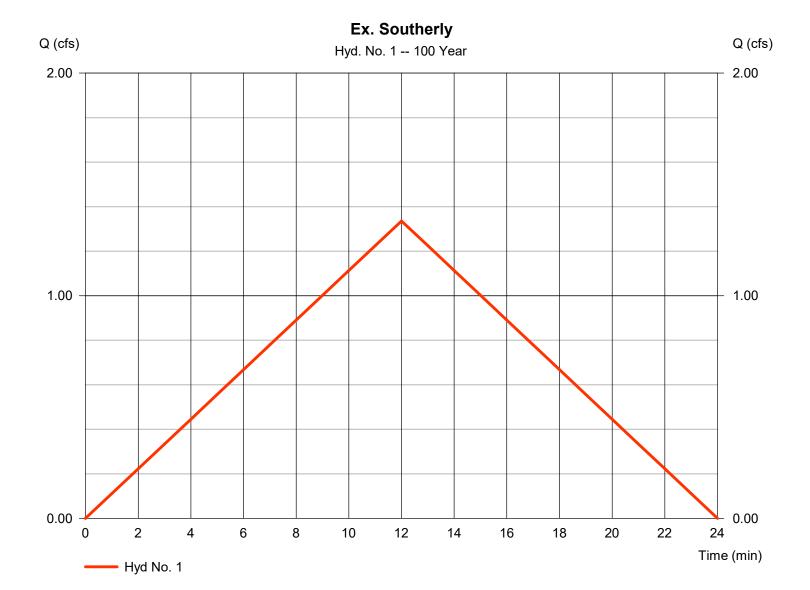
Hyd. No. 1

Ex. Southerly

Hydrograph type = 1.336 cfs= Rational Peak discharge Storm frequency = 100 yrsTime to peak = 12 min Time interval = 1 min Hyd. volume = 962 cuft Drainage area Runoff coeff. = 1.950 ac= 0.1

Intensity = 6.850 in/hr Tc by User = 12.00 min

IDF Curve = Railroad Street, Salisbury, CT ADSTE/GenveinhDFfact = 1/1



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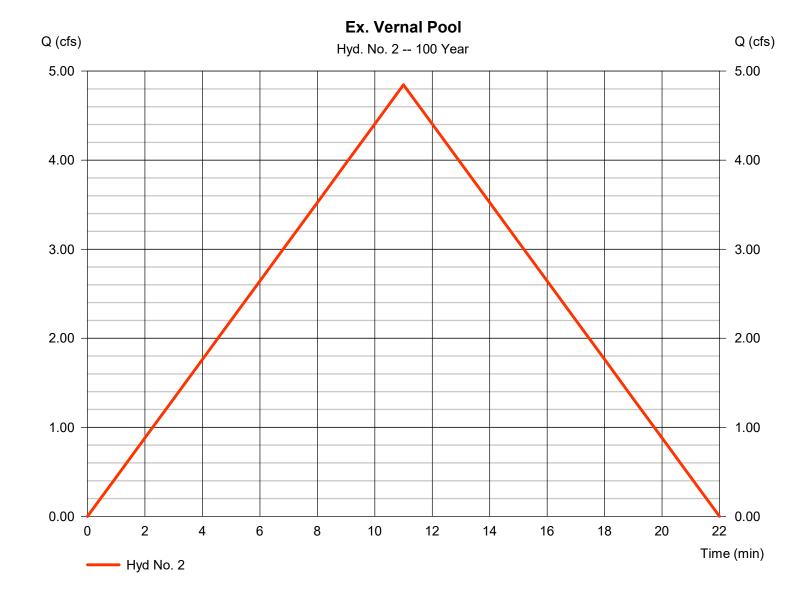
Monday, 11 / 20 / 2023

Hyd. No. 2

Ex. Vernal Pool

Hydrograph type = Rational Peak discharge = 4.846 cfsStorm frequency = 100 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 3,199 cuftDrainage area Runoff coeff. = 4.220 ac= 0.16Tc by User Intensity = 7.178 in/hr= 11.00 min

IDF Curve = Railroad Street, Salisbury, CT ADSTE/Renovemb10 Fract = 1/1



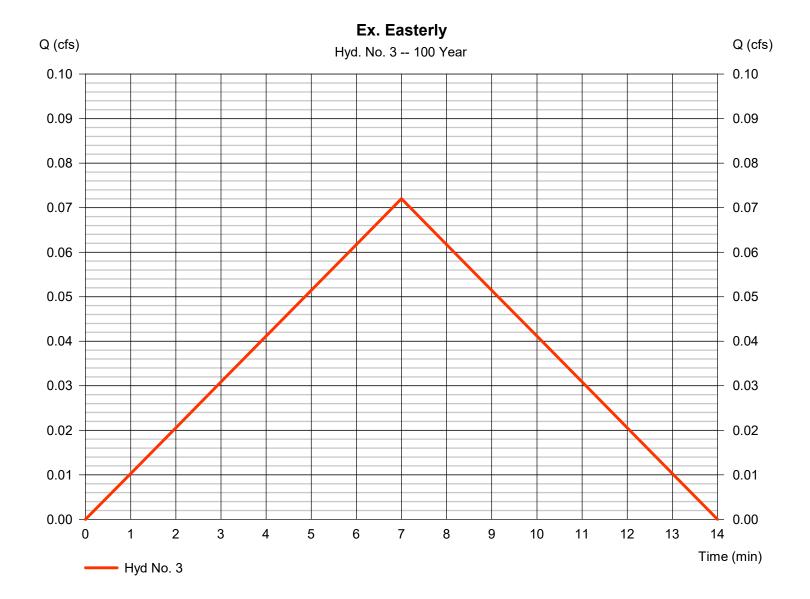
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Monday, 11 / 20 / 2023

Hyd. No. 3

Ex. Easterly

Hydrograph type = Rational Peak discharge = 0.072 cfsStorm frequency = 100 yrsTime to peak = 7 min Time interval = 1 min Hyd. volume = 30 cuft Runoff coeff. = 0.1Drainage area = 0.080 acTc by User $= 7.00 \, \text{min}$ Intensity = 9.001 in/hr= Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact IDF Curve = 1/1



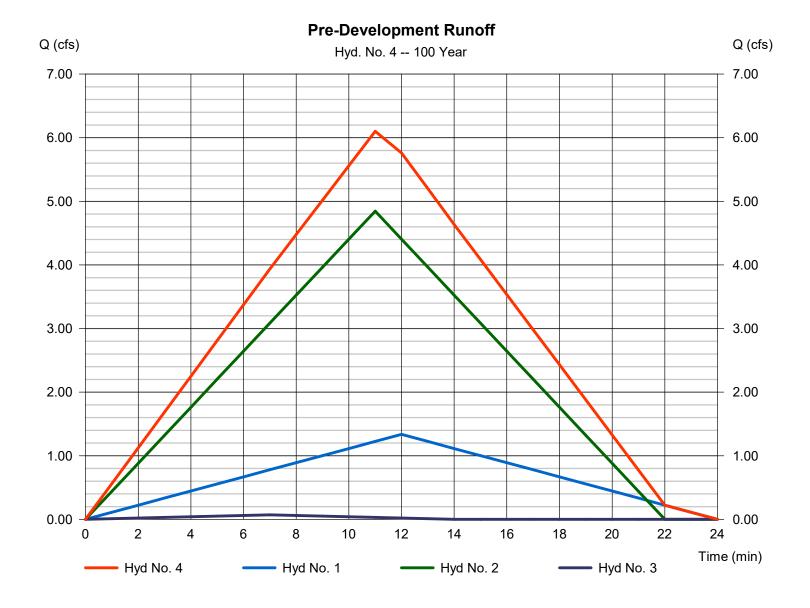
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Hyd. No. 4

Pre-Development Runoff

Hydrograph type = Combine Peak discharge = 6.102 cfsStorm frequency Time to peak = 100 yrs= 11 min Time interval = 1 min Hyd. volume = 4,191 cuft Inflow hyds. = 1, 2, 3Contrib. drain. area = 6.250 ac



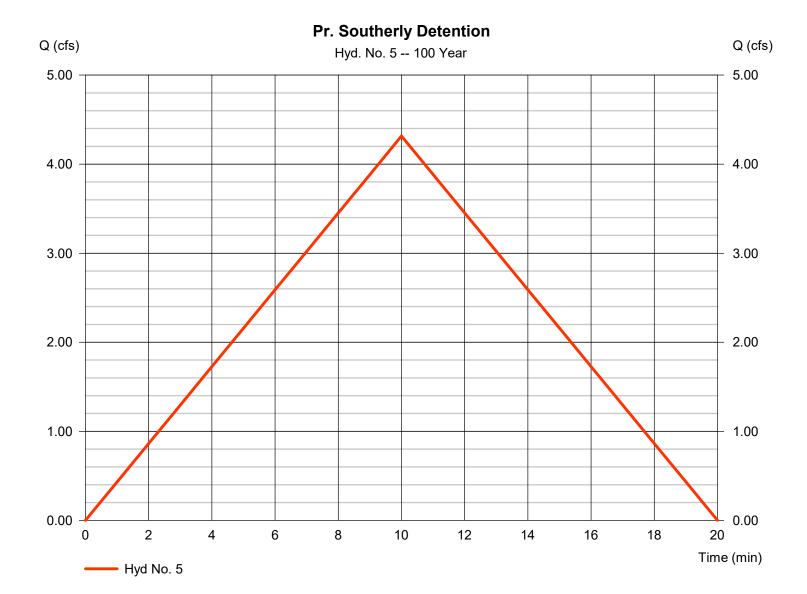
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Monday, 11 / 20 / 2023

Hyd. No. 5

Pr. Southerly Detention

Hydrograph type Peak discharge = 4.316 cfs= Rational Storm frequency = 100 yrsTime to peak = 10 min Time interval = 1 min Hyd. volume = 2,589 cuftRunoff coeff. Drainage area = 1.330 ac= 0.43Tc by User Intensity = 7.546 in/hr $= 10.00 \, \text{min}$ = Railroad Street, Salisbury, CT ADSTE/Renovember IDF Curve = 1/1



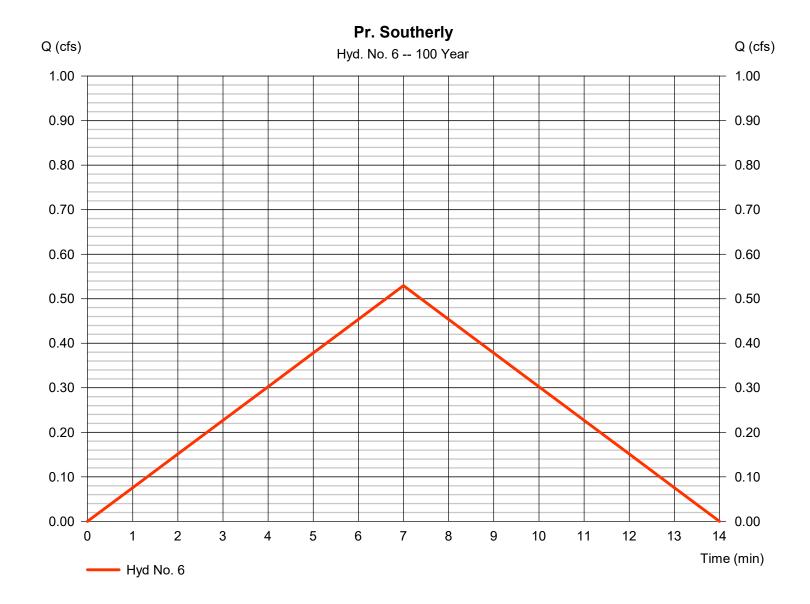
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Hyd. No. 6

Pr. Southerly

Hydrograph type = Rational Peak discharge = 0.529 cfsStorm frequency Time to peak = 100 yrs= 7 min Time interval = 1 min Hyd. volume = 222 cuft Drainage area Runoff coeff. = 0.490 ac= 0.12Tc by User Intensity = 9.001 in/hr $= 7.00 \, \text{min}$ = Railroad Street, Salisbury, CT ADSTE/Renc/tent/DFfact **IDF** Curve = 1/1



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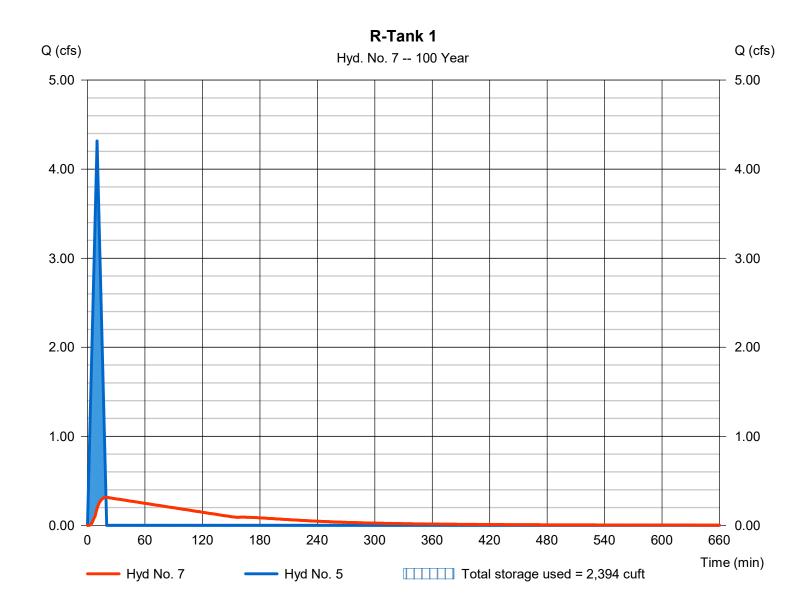
Monday, 11 / 20 / 2023

Hyd. No. 7

R-Tank 1

Hydrograph type Peak discharge = 0.315 cfs= Reservoir Storm frequency = 100 yrsTime to peak = 19 min Time interval = 1 min Hyd. volume = 2,541 cuftMax. Elevation Inflow hyd. No. = 5 - Pr. Southerly Detention $= 673.56 \, \text{ft}$ = Southerly Watershed R-Tank 1Max. Storage Reservoir name = 2,394 cuft

Storage Indication method used.



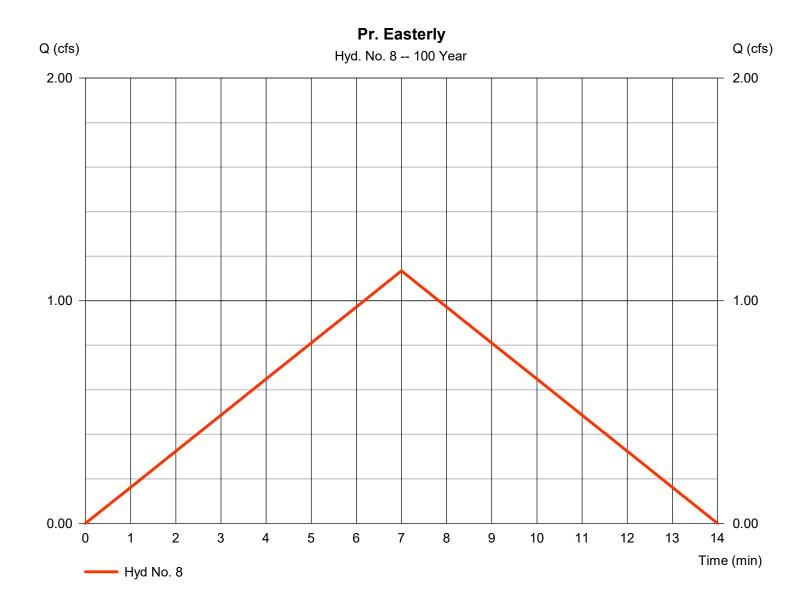
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Monday, 11 / 20 / 2023

Hyd. No. 8

Pr. Easterly

= 1.134 cfsHydrograph type = Rational Peak discharge Storm frequency = 7 min = 100 yrsTime to peak Time interval = 1 min Hyd. volume = 476 cuft = 0.42Runoff coeff. Drainage area = 0.300 acTc by User $= 7.00 \, \text{min}$ Intensity = 9.001 in/hr= Railroad Street, Salisbury, CT ADSE/Renovembn Fact IDF Curve = 1/1



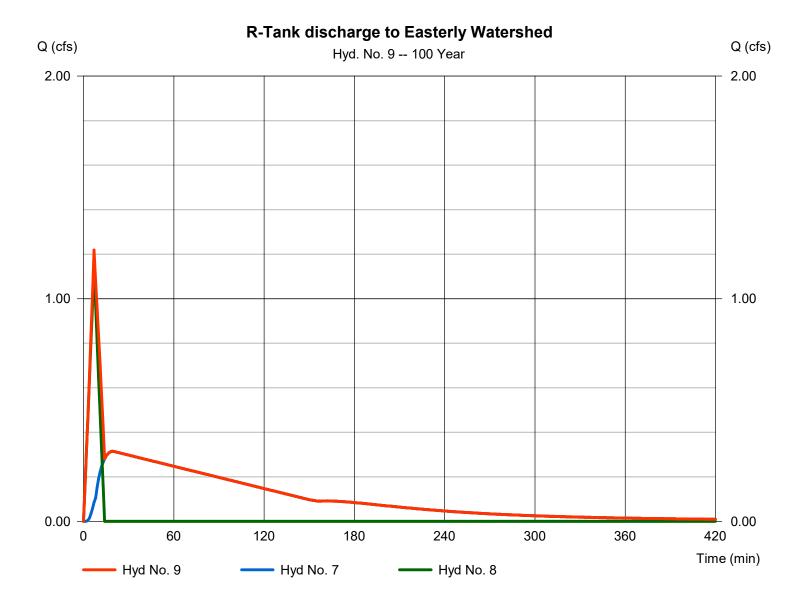
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Monday, 11 / 20 / 2023

Hyd. No. 9

R-Tank discharge to Easterly Watershed

= 1.219 cfsHydrograph type = Combine Peak discharge Storm frequency Time to peak = 100 yrs= 7 min Time interval = 1 min Hyd. volume = 3,018 cuftInflow hyds. = 7,8 Contrib. drain. area = 0.300 ac



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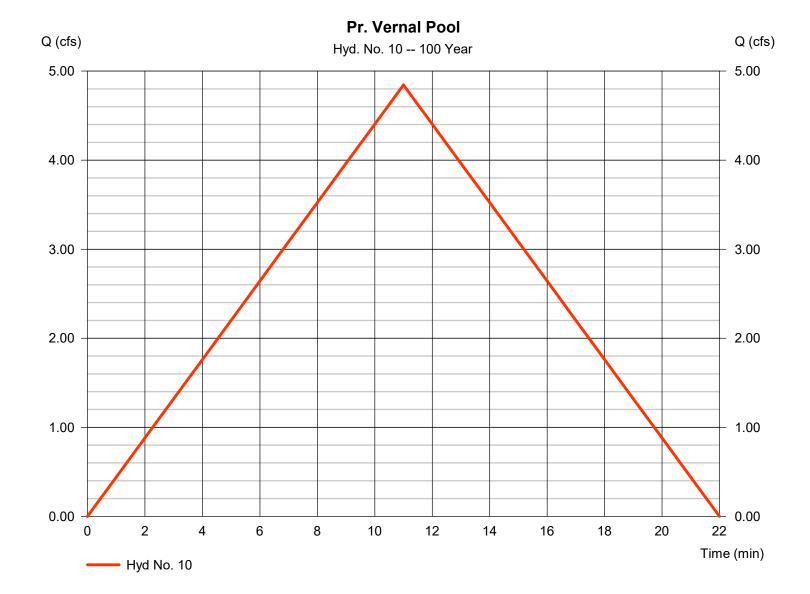
Monday, 11 / 20 / 2023

Hyd. No. 10

Pr. Vernal Pool

Hydrograph type = Rational Peak discharge = 4.845 cfsStorm frequency = 100 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 3,198 cuftDrainage area Runoff coeff. = 3.750 ac= 0.18Tc by User Intensity = 7.178 in/hr= 11.00 min

IDF Curve = Railroad Street, Salisbury, CT ADSE/RenovenhDFact = 1/1



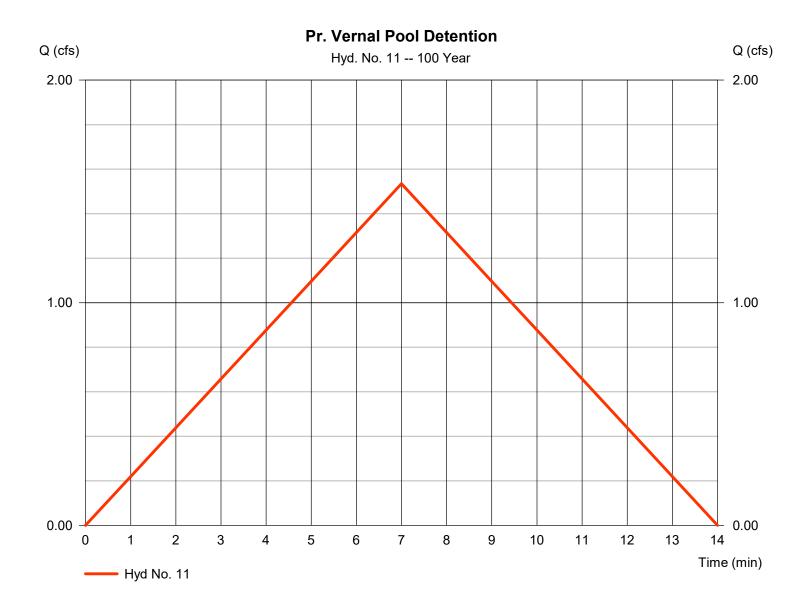
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Monday, 11 / 20 / 2023

Hyd. No. 11

Pr. Vernal Pool Detention

Hydrograph type = Rational Peak discharge = 1.535 cfsStorm frequency Time to peak = 100 yrs= 7 min Time interval = 1 min Hyd. volume = 645 cuft Drainage area Runoff coeff. = 0.31= 0.550 acTc by User $= 7.00 \, \text{min}$ Intensity = 9.001 in/hr= Railroad Street, Salisbury, CT ADSTE/Renovember IDF Curve = 1/1



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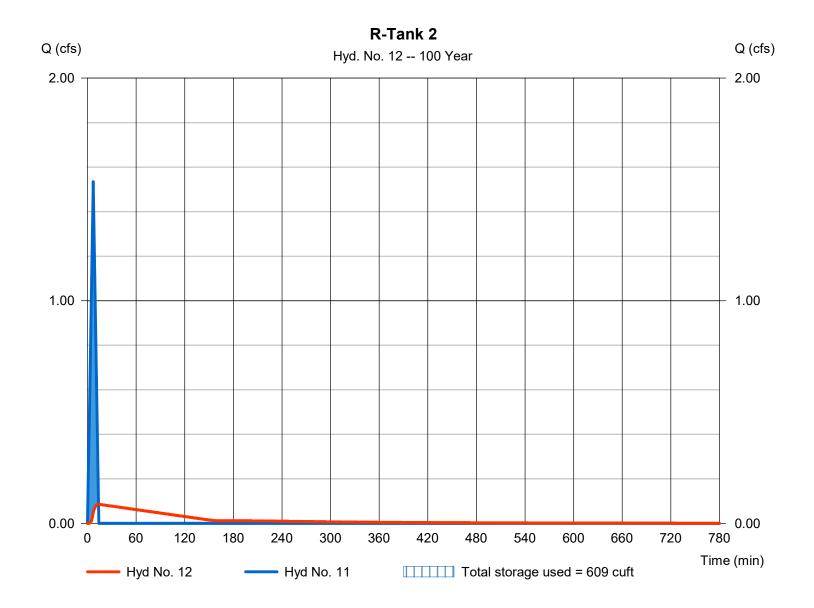
Monday, 11 / 20 / 2023

Hyd. No. 12

R-Tank 2

Hydrograph type = Reservoir Peak discharge = 0.086 cfsStorm frequency = 100 yrsTime to peak = 14 min Time interval = 1 min Hyd. volume = 606 cuft Inflow hyd. No. = 11 - Pr. Vernal Pool Detention Max. Elevation = 672.56 ft= Vernal Pool Watershed R-Tank/Pax. Storage Reservoir name = 609 cuft

Storage Indication method used.



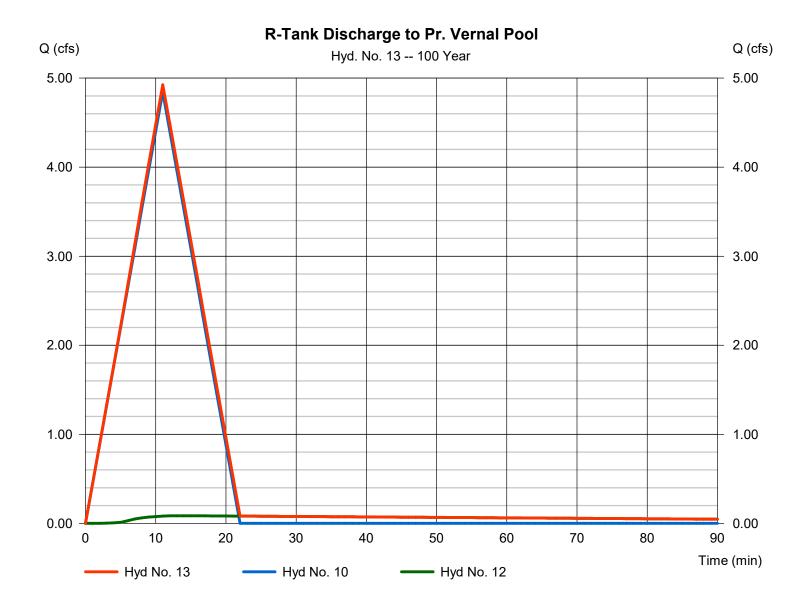
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Monday, 11 / 20 / 2023

Hyd. No. 13

R-Tank Discharge to Pr. Vernal Pool

Hydrograph type = Combine Peak discharge = 4.926 cfsStorm frequency = 100 yrsTime to peak = 11 min Time interval = 1 min Hyd. volume = 3,804 cuftInflow hyds. Contrib. drain. area = 3.750 ac= 10, 12



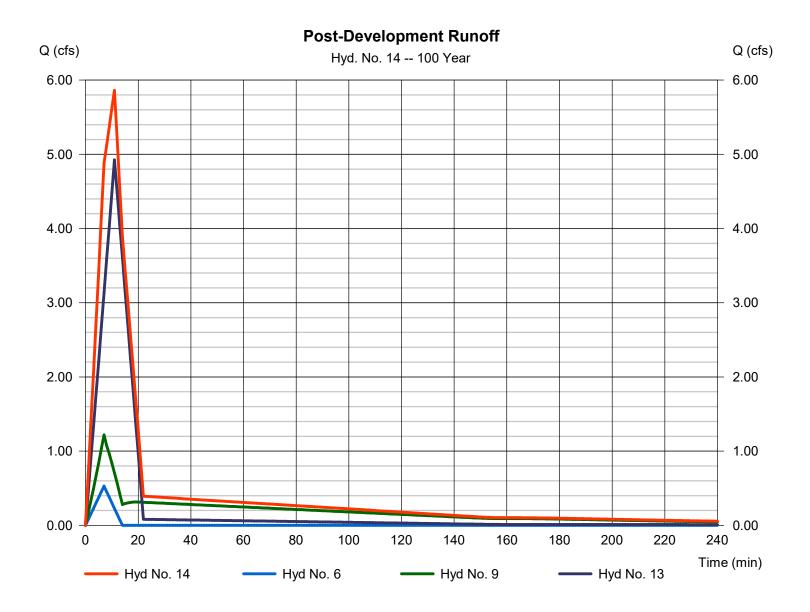
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Monday, 11 / 20 / 2023

Hyd. No. 14

Post-Development Runoff

Hydrograph type = Combine Peak discharge = 5.860 cfsStorm frequency Time to peak = 100 yrs= 11 min Time interval = 1 min Hyd. volume = 7,044 cuftInflow hyds. Contrib. drain. area = 6, 9, 13= 0.490 ac



D. Pond Report

Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Monday, 11 / 20 / 2023

Pond No. 1 - Southerly Watershed R-Tank 1

Pond Data

UG Chambers -Invert elev. = 672.50 ft, Rise x Span = 1.44 x 30.19 ft, Barrel Len = 75.07 ft, No. Barrels = 1, Slope = 0.00%, Headers = No

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	672.50	n/a	0	0
0.14	672.64	n/a	326	326
0.29	672.79	n/a	327	653
0.43	672.93	n/a	326	979
0.58	673.08	n/a	326	1,306
0.72	673.22	n/a	326	1,632
0.86	673.36	n/a	327	1,959
1.01	673.51	n/a	326	2,285
1.15	673.65	n/a	326	2,611
1.30	673.80	n/a	327	2,938
1.44	673.94	n/a	326	3,264

Culvert / Orifice Structures Weir Structures [B] [PrfRsr] [A] [B] [C] [D] [A] [C] = 4.00 0.00 0.00 0.00 = 0.000.00 0.00 0.00 Crest Len (ft) Rise (in) Span (in) = 4.000.00 0.00 0.00 Crest El. (ft) = 0.000.00 0.00 0.00 No. Barrels = 1 0 0 0 Weir Coeff. = 3.333.33 3.33 3.33 0.00 0.00 0.00 Weir Type Invert El. (ft) = 672.50 = ---= 25.00 0.00 0.00 0.00 Multi-Stage = No No No No Length (ft) 0.00 0.00 Slope (%) = 0.25n/a .013 N-Value = .011 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 0.000 (by Wet area) = n/a No No No = 0.00Multi-Stage TW Elev. (ft)

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	CIv A cfs	Clv B cfs	CIv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	672.50	0.00										0.000
0.14	326	672.64	0.04 oc										0.035
0.29	653	672.79	0.09 oc										0.088
0.43	979	672.93	0.14 oc										0.143
0.58	1,306	673.08	0.20 oc										0.196
0.72	1,632	673.22	0.24 oc										0.238
0.86	1,959	673.36	0.27 oc										0.273
1.01	2,285	673.51	0.30 oc										0.305
1.15	2,611	673.65	0.33 oc										0.333
1.30	2,938	673.80	0.36 oc										0.359
1.44	3,264	673.94	0.38 oc										0.384

Pond Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2024

Monday, 11 / 20 / 2023

Pond No. 2 - Vernal Pool Watershed R-Tank 2

Pond Data

UG Chambers -Invert elev. = 671.50 ft, Rise x Span = 1.44 x 14.44 ft, Barrel Len = 39.87 ft, No. Barrels = 1, Slope = 0.00%, Headers = No

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	671.50	n/a	0	0
0.14	671.64	n/a	83	83
0.29	671.79	n/a	83	166
0.43	671.93	n/a	83	249
0.58	672.08	n/a	83	332
0.72	672.22	n/a	83	415
0.86	672.36	n/a	83	498
1.01	672.51	n/a	83	580
1.15	672.65	n/a	83	663
1.30	672.80	n/a	83	746
1.44	672.94	n/a	83	829

Culvert / Orifice Structures Weir Structures [B] [PrfRsr] [A] [B] [C] [D] [A] [C] = 4.00 0.00 0.00 0.00 = 0.000.00 0.00 0.00 Rise (in) Crest Len (ft) Span (in) = 4.000.00 0.00 0.00 Crest El. (ft) = 0.000.00 0.00 0.00 No. Barrels = 1 0 0 0 Weir Coeff. = 3.333.33 3.33 3.33 = 671.50 0.00 0.00 0.00 Weir Type Invert El. (ft) = ---= 5.00 0.00 0.00 0.00 Multi-Stage = No No No No Length (ft) = 0.25 0.00 0.00 Slope (%) n/a .013 N-Value = .110 .013 n/a Orifice Coeff. = 0.600.60 0.60 0.60 Exfil.(in/hr) = 0.000 (by Wet area) = n/a No No No = 0.00Multi-Stage TW Elev. (ft)

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	CIv A cfs	CIv B cfs	CIv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	671.50	0.00										0.000
0.14	83	671.64	0.00 oc										0.004
0.29	166	671.79	0.01 oc										0.012
0.43	249	671.93	0.03 oc										0.033
0.58	332	672.08	0.05 oc										0.050
0.72	415	672.22	0.06 oc										0.063
0.86	498	672.36	0.07 oc										0.073
1.01	580	672.51	0.08 oc										0.083
1.15	663	672.65	0.09 oc										0.091
1.30	746	672.80	0.10 oc										0.098
1.44	829	672.94	0.11 oc										0.105

Ε.	Rain Garden Calculations

Building	Roof Area (ft ²)	Volume of 1 inch of Runoff (ft ³)				
1	1088	91				
2	1144	95				
3	1088	91				
4	1484	124				
5	1756	146				
6	1556	130				
7	2295	191				
8	1556	130				
9	1756	146				

Rain Garden near Building 9

Contour Area

677.75 352 678.5 631

Difference = 0.75 Average = 491 Volume Provided = 369 ft³

Volume Required = 146 ft³

Rain Garden near Building 2

Contour Area

677.5 190 678 392

Difference = 0.5 Average = 291 Volume Provided = 146 ft³

Volume Required = 95 ft³

Rain Garden near Building 3 and 4

Contour Area

675 524 675.5 746

Difference = 0.5 Average = 635 Volume Provided = 318 ft³

Volume Required = 215 ft³

Rain Garden near Building 5

Contour Area

675.25 136 676 315

Difference = 0.75 Average = 226 Volume Provided = 169 ft³

Volume Required = 146 ft³

Rain Garden near Building 6 and 7

Contour Area

674.25 311 675 607

Difference = 0.75 Average = 459 Volume Provided = 344 ft³

Volume Required = 321 ft³